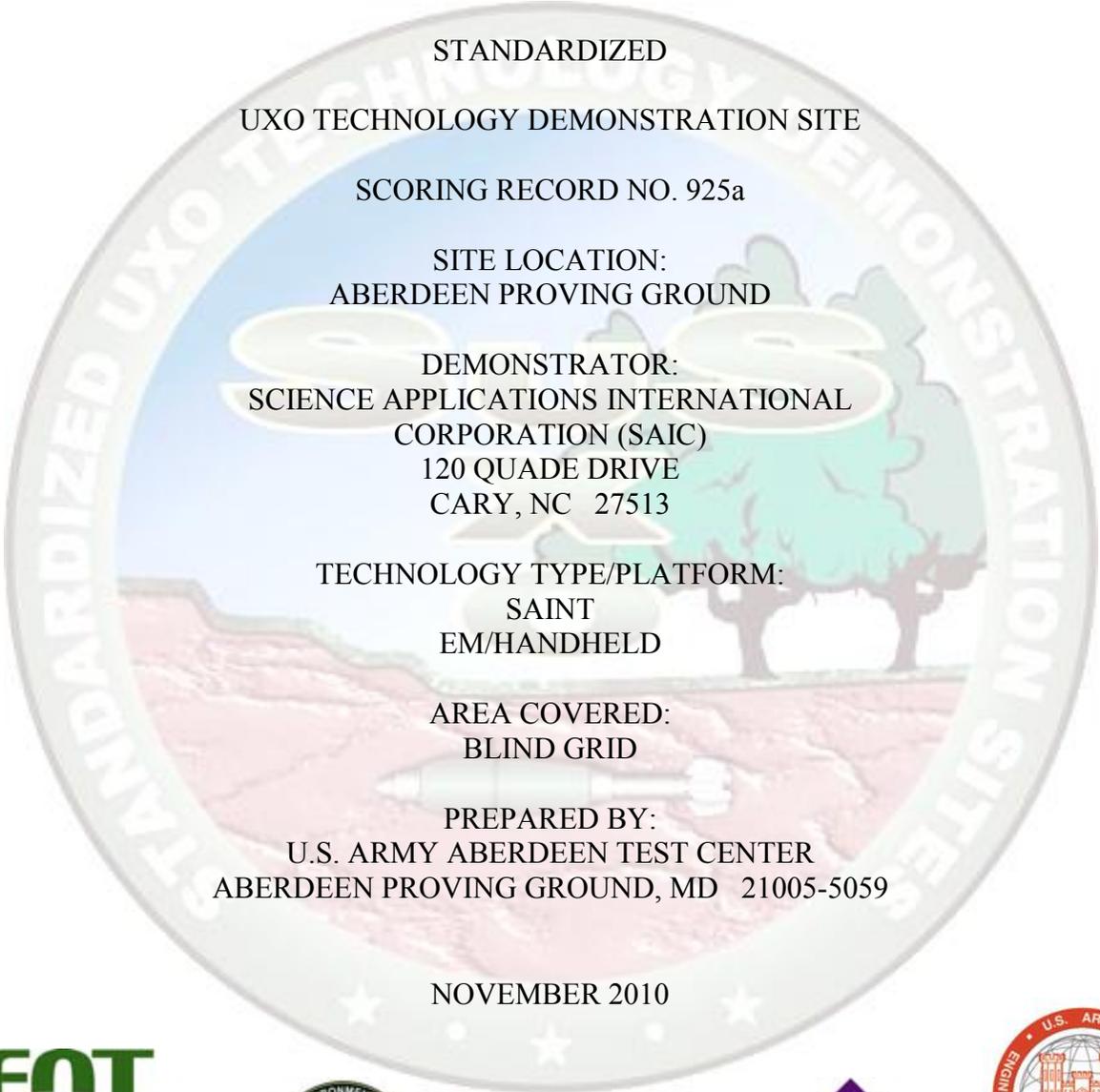




AD NO. _____
 DTC PROJECT NO. 8-CO-160-UXO-021
 REPORT NO. ATC 10419



STANDARDIZED

UXO TECHNOLOGY DEMONSTRATION SITE

SCORING RECORD NO. 925a

SITE LOCATION:
 ABERDEEN PROVING GROUND

DEMONSTRATOR:
 SCIENCE APPLICATIONS INTERNATIONAL
 CORPORATION (SAIC)
 120 QUADE DRIVE
 CARY, NC 27513

TECHNOLOGY TYPE/PLATFORM:
 SAINT
 EM/HANDHELD

AREA COVERED:
 BLIND GRID

PREPARED BY:
 U.S. ARMY ABERDEEN TEST CENTER
 ABERDEEN PROVING GROUND, MD 21005-5059

NOVEMBER 2010



Prepared for:
 SERDP/ESTCP
 MUNITIONS MANAGEMENT
 ARLINGTON, VA 22203

U.S. ARMY DEVELOPMENTAL TEST COMMAND
 ABERDEEN PROVING GROUND, MD 21005-5055

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SECTION 1. GENERAL INFORMATION

1.1 BACKGROUND

Technologies under development for the detection and discrimination of military munitions (MM) (i.e. unexploded ordnance (UXO) and discarded military munitions (DMM)) require testing so that performance can be characterized. To that end, Standardized Test Sites have been developed at Aberdeen Proving Ground (APG), Maryland, and U.S. Army Yuma Proving Ground (YPG), Arizona. These test sites provide a diversity of geology, climate, terrain, and weather as well as diversity in munitions and clutter. Testing at these sites is independently administered and analyzed by the Government for the purposes of characterizing technologies, tracking performance with system development, comparing performance of different systems, and comparing performance in different environments (ref 1).

The Standardized UXO Technology Demonstration Site Program is a multiagency program spearheaded by the U.S. Army Environmental Command (USAEC). The U.S. Army Aberdeen Test Center (ATC) and the U.S. Army Corps of Engineers Engineering Research and Development Center (ERDC) provide programmatic support. The program is being funded and supported by the Environmental Security Technology Certification Program (ESTCP), the Strategic Environmental Research and Development Program (SERDP), and the U.S. Army Environmental Quality Technology (EQT) Program.

1.2 SCORING OBJECTIVES

The objective in the Standardized UXO Technology Demonstration Site Program is to evaluate the detection and discrimination capabilities of a given technology under various field and soil conditions. Inert munitions and clutter items are positioned in various orientations and depths in the ground.

The evaluation objectives are as follows:

- a. To determine detection and discrimination effectiveness under realistic scenarios with various targets, geology, clutter, density, topography, and vegetation.
- b. To determine cost, time, and workforce requirements to operate the technology.
- c. To determine the demonstrator's ability to analyze survey data in a timely manner and provide prioritized Target Lists with associated confidence levels.
- d. To provide independent site management to enable the collection of high quality, ground-truth (GT), geo-referenced data for post-demonstration analysis.

1.2.1 Scoring Methodology

a. The scoring of the demonstrator's performance is conducted in two stages: response stage and discrimination stage. For both stages, the probability of detection (P_d) and the false alarms are reported as receiver-operating characteristic (ROC) curves. False alarms are divided into those anomalies that correspond to emplaced clutter items, measuring the probability of clutter detection (P_{cd}) or the probability of false positive (P_{fp}). Those that do not correspond to any known item are termed background alarms. The background alarms are addressed as either probability of background alarm (P_{ba}) or background alarm rate (BAR).

b. The response stage scoring evaluates the ability of the system to detect emplaced targets without regard to ability to discriminate munitions from other anomaly sources. For the blind grid response stage, the demonstrator provides a target response from each and every grid square along with a threshold below which target responses are deemed insufficient to warrant further investigation. This list is generated with minimal processing and, since a value is provided for every grid square, includes amplitudes both above and below the system noise level. For the open field, the demonstrator provides a list of all anomalies deemed to exceed a demonstrator selected target detection threshold. An item (either munition or clutter) is counted as detected if a demonstrator indicates an anomaly within a specified distance (Halo Radius (R_{halo})) of a ground truth item.

c. The discrimination stage evaluates the demonstrator's ability to correctly identify munitions as such and to reject clutter. For the blind grid discrimination stage, the demonstrator provides the output of the discrimination stage processing for each grid square. For the open field, the demonstrator provides the output of the discrimination stage processing for anomaly reported in the response stage. The values in these lists are prioritized based on the demonstrator's determination that a location is likely to contain munitions. Thus, higher output values are indicative of higher confidence that a munitions item is present at the specified location. For digital signal processing, priority ranking is based on algorithm output. For other discrimination approaches, priority ranking may be based on rule sets or human judgment. The demonstrator also specifies the threshold in the prioritized ranking that provides optimum performance (i.e., that is expected to retain all detected munitions and reject the maximum amount of clutter).

d. The demonstrator is also scored on efficiency and rejection ratios, which measure the effectiveness of the discrimination stage processing. The goal of discrimination is to retain the greatest number of munitions detections from the anomaly list, while rejecting the maximum number of anomalies arising from nonmunitions items. Efficiency measures the fraction of detected munitions retained after discrimination, while the rejection ratio measures the fraction of false alarms rejected. Both measures are defined relative to the maximum number of munitions detectable by the sensor and its accompanying clutter detection/false positive rate or BAR.

e. Based on configuration of the GT at the standardized sites and the defined scoring methodology, in some cases, there exists the possibility of having anomalies within overlapping halos and/or multiple anomalies within halos. In these cases, the following scoring logic is implemented:

(1) In situations where multiple anomalies exist within a single R_{halo} , the anomaly with the strongest response or highest ranking will be assigned to that particular GT item. If the responses or rankings are equal, then the anomaly closest to the GT item will be assigned to the GT item. Remaining anomalies are retained and scored until all matching is complete.

(2) Anomalies located within any R_{halo} that do not get associated with a particular GT item are excess alarms and will be disregarded.

f. In some cases, groups of closely spaced munitions have overlapping halos. The following scoring logic is implemented (app A, fig. A-1 through A-9):

- (1) Overall site scores (i.e., P_d) will consider only isolated munitions and clutter items.
- (2) GT items that have overlapping halos (both munitions and clutter) will form a group and groups may form chains.
- (3) Groups will have a complex halos composed of the composite halos of all its GT items.
- (4) Groups will have three scoring factors: groups found, groups identified, and group coverage. Scores will be based on 1:1 matches of anomalies and GT.
 - (a) Groups Found (Found): the number of groups that have one or more GT items matched divided by the total number of groups. Demonstrators will be credited with detecting a group if any item within the group is matched to an anomaly in their lists.
 - (b) Groups Identified (ID): the number of groups that have two or more GT items matched divided by the total number of groups. Demonstrators will be credited with identifying that a group is present if multiple items within the composite halo are matched to anomalies in their lists.
 - (c) Group Coverage (Coverage): the number of GT items matched within groups divided by the total number of GT items within groups. This metric measures the demonstrator accuracy in determining the number of anomalies within a group. If five items are present and only two anomalies are matched, the demonstrator will score 0.4. If all five are matched, the demonstrator will score 1.0.
- (5) Location error will not be reported for groups.

(6) Demonstrators will not be asked to call out groups in their scoring submissions. If multiple anomalies are indicated in a small area, the demonstrator will report all individual anomalies.

(7) Excess alarms within a halo will be disregarded.

g. All scoring factors are generated utilizing the Standardized UXO Probability and Plot Program, version 4.

1.2.2 Scoring Factors

Factors to be measured and evaluated as part of this demonstration include:

a. Response stage ROC curves:

(1) Probability of detection (P_d^{res}).

(2) Probability of clutter detection (P_{cd}).

(3) Background alarm rate (BAR^{res}) or probability of background alarm ($P_{\text{ba}}^{\text{res}}$).

b. Discrimination stage ROC curves:

(1) Probability of detection (P_d^{disc}).

(2) Probability of false positive (P_{fp}).

(3) Background alarm rate (BAR^{disc}) or probability of background alarm ($P_{\text{ba}}^{\text{disc}}$).

c. Metrics:

(1) Efficiency (E).

(2) False positive rejection rate (R_{fp}).

(3) Background alarm rejection rate (R_{ba}).

d. Other:

(1) Probability of detection by size, depth, and density.

(2) Classification by type (i.e., 20-, 40-, 105-mm, etc.).

(3) Location accuracy for single munitions.

- (4) Equipment setup, calibration time, and corresponding worker-hour requirements.
- (5) Survey time and corresponding worker-hour requirements.
- (6) Reacquisition/resurvey time and worker-hour requirements (if any).
- (7) Downtime due to system malfunctions and maintenance requirements.

SECTION 2. DEMONSTRATION

2.1 DEMONSTRATOR INFORMATION

2.1.1 Demonstrator Point of Contact (POC) and Address

Address: Science Applications International Corporation (SAIC)
120 Quade Drive
Cary, NC 27513

2.1.2 System Description (provided by demonstrator)

a. SAIC utilized a Geonics EM61HH-MK2 sensor. The EM61HH-MK2 is a hand held complement to the EM61-MK2, providing greater sensitivity to smaller targets at shallow depths. Data are collected from an air-core, 17-cm diameter, single receive coil at four time gates, geometrically spaced in time from 147 μ s to 613 μ s, after transmitter turnoff. With a narrower spatial focus than the standard EM61-MK2, the EM61HH-MK2 is relatively less sensitive to sources of potential interference. The narrower focus also provides enhanced target resolution and, consequently, improves discrimination of multiple targets. Effective cued identification using the EM61HH-MK2 has been demonstrated by ATEC in ESTCP project 200108 (Handheld Sensor for Unexploded Ordnance Discrimination). As reported at the 2002 SERDP/ESTCP Partners in Environmental Technology Symposium, the technology was demonstrated at a Brownfield Redevelopment site and achieved excellent results in discriminating between UXO items (37-mm, 47-mm, and 75-mm projectiles) and various industrial and cultural clutter items. For that demonstration, the sensor positioning problem was solved by collecting data on a fixed grid over the target, using a template laid on the ground.

b. For recording the 3-D position of the sensor, we will utilize a small area inertial navigation tracking (SAINT) system (fig. 1) that has been developed by ENSCO, in part, under MM-0604. It is a stand-alone unit that can be attached to virtually any geophysical sensing system. The inertial navigation tracking system consists of a Honeywell HG1900 inertial measurement unit (IMU) and a LEICA digital magnetic compass (DMC). The Honeywell HG1900 IMU consists of orthogonally aligned micro electro-mechanical systems (MEMS) accelerometers and gyroscopes that record 3-axis acceleration and rotation rates, respectively, enclosed in an 8-cubic-inch container. The LEICA DMC is employed to aid the IMU and constrain heading drift. The digital magnetic compass measures the strength and direction of a magnetic field and can be used to determine magnetic north in an environment free of additional magnetic fields. With the exception of batteries, a tripod stand, and the post-processing personal computer (PC), all components of SAINT are packaged into a single enclosure.



Figure 1. SAIC SAINT/hand held.

c. Support equipment required. For the sensor, overnight storage, protected from the elements, and access to electrical power for battery charging are required. Storage, power, and workspace for the data quality control analyst can be located in the building on-site.

d. Frequency and radio utilization involve a local interrogation system and do not utilize a GPS system or require hand held radios.

2.1.3 Data Processing Description (provided by demonstrator)

Targets for this demonstration will be chosen based on the signal expected for each item at the maximum depth of interest. SAIC will determine the minimum sensor response versus depth for each of the three items of interest in this demonstration prior to the demonstration.

a. What kind of pre-processing (if any) is applied to the raw data (e.g., filtering)?

The preprocessing for the SAINT exploits the operational requirement that the start and stop locations of the SAINT hardware be identical. The operator can free-navigate for 30 seconds, at which time the unit must be returned to the same place it started. A tripod is used to simplify the return of the hardware to the identical location. Upon completion of the zero velocity update (ZUPT), a blue indicator light illuminates on the SAINT enclosure, signifying that the operator can free-navigate when ready.

The post-processing software has been mostly automated and includes a graphical user interface (GUI) that requires the user to select the EM61HH-MK2 data and IMU data files for processing and the periods to process. The processing consists of the following components:

A pre-filter for detection of ZUPT intervals.

Navigation equations and a Kalman filter.

An R-T-S smoother.

A component to translate the IMU position and attitude to the geophysical sensor, based on the static 3-D position and orientation of offset vectors.

A component to interpolate the sensor position and attitude (recorded at up to 600 Hz) to the recorded EM61 times (recorded at approximately 15 Hz).

b. What is the format of the raw data, both pre- and post-processing (e.g., ASCII, binary)? ASCII.

c. What algorithm is used for detection (e.g. peaks of signal surpassing threshold)? Signal peak.

d. Why is this algorithm used and not others? This approach is similar to others that assume the source can be modeled as a simple dipole.

e. On what principles is the algorithm based (e.g., statistical models, heuristic rules)? Physics-inspired dipole model.

f. What tunable parameters (if any) are used in the detection process (e.g. threshold on signal amplitude, window length, filter coefficients)? None.

g. What are the final values of all tunable parameters for the detection algorithm? None

Parameter Estimation.

The EM61HH-MK2 data are inverted using the standard induced dipole response model, wherein the effect of eddy currents set up in the target by the primary field is represented by a set of three orthogonal magnetic dipoles at the target location. The measured signal is a linear function of the induced dipole moment m , which can be expressed in terms of a time dependent polarizability tensor B as:

$$m = UBU^T H_0$$

where: U is the transformation matrix between the physical coordinate directions and the principal axes of the target, and H_0 is the primary field strength at the target. The eigenvalues $\beta_i(t)$ of the polarizability tensor are the principal axis polarizabilities.

Given a set of measurements of the target response with varying geometries, or look angles, at the target, the data can be inverted to determine the (X, Y, Z) location of the target, the orientation of its principal axes (ψ , θ , ϕ), and the principal axis polarizabilities (β_1 , β_2 , β_3). The basic idea is to search out the set of nine parameters (X, Y, Z, ψ , θ , ϕ , β_1 , β_2 , β_3) that minimize the difference between the measured responses and those calculated using the dipole response model.

In some situations (depending on target size, orientation, and distance from the sensor head) there is a bit of ambiguity regarding the correct values of the β 's and the depth. SAIC suspects that this is due to failure of the dipole response model to faithfully reproduce the signal when the dimensions of the target are comparable with distances over which there are significant changes in the primary field (and the reciprocal received field). For most UXO, there is one large β corresponding to the axial response and two smaller, equal β 's corresponding to transverse responses. With ordnance items on a test stand, we find that the depth at which the secondary β 's are equal is not always the depth that minimizes the RMS deviation between the data and the dipole model. Consequently, for the grid template, the EM data will be processed by systematically stepping through depths ranging from 5 cm to 100 cm below the ground level. As a function of depth, we will fit the array data to a dipole response model using a least squares procedure. SAIC will then look at the best fit polarizations and residual error as functions of depth to find the final estimated values.

There are several additional complications in inverting the EM61HH-MK2 data combined with the SAINT. The first is the added requirement for modeling the dynamic time response of the sensor. The receiver output of this sensor is analog integrated with a filter that both shifts and distorts the response of the sensor. This filter has been added to the forward model used by the inversion algorithm. It is possible that this filter is sufficiently distorting signal shape to limit the inversion process. The second complication is the sensor bias drift. Over minutes of data collection, the zero level of the sensor will change. The data collected here starts with the sensor on a metal tripod with an unknown offset. It then moves back and forth over an object, perhaps reaching zero at points, perhaps not. For this reason, an offset parameter has been added to the data inversion.

Not every target detected during the magnetometer survey will have a strong enough EM61HH response to support extraction of target polarizabilities. All of the data will be run through the inversion routines, and the results will be manually screened to identify those targets that cannot be reliably classified. Several criteria will be used in this process: signal strength relative to background, dipole fit error (difference between data and model fit to data), and the visual appearance of the polarizability curves.

SAIC will compare the model parameters from the SAINT-positioned data to the grid template-positioned data for all common anomalies that support extraction of target polarizabilities. The size of the target can be estimated from the sum of the targets' response coefficients. In order to parameterize the shape information, we will calculate the aspect ratio and an asymmetry metric. The aspect ratio is defined as the ratio of the largest response coefficient to the mean of the remaining two. The asymmetry metric is defined as the difference

between the two smaller response coefficients divided by the larger of the two. Expressed this way, the asymmetry metric ranges from 0 to 1, where 0 indicates that the two smaller response coefficients are equal and therefore axially symmetric, and a value of 1 essentially indicates that the smaller response coefficient is equal to zero. The majority of ordnance at this site will ideally have aspect ratios of 2:6 and an asymmetry value of close to 0.

a. Which characteristics will be extracted from each detected item and input to the discrimination algorithm (e.g., depth, size, polarizability coefficients, fit quality)? Principal axis polarizabilities and fit error statistic.

b. Why have these characteristics been chosen and not others (e.g., empirical evidence of their ability to help discriminate, inclusion in a theoretical tradition)? They are intrinsic to the target.

c. How are these characteristics estimated (e.g. least-mean-squares fit to a dipole model), including the equations that are used for parameter estimation? Least-mean-squares fit to a dipole model, see above.

d. What tunable parameters (if any) are used in the characterization process? (e.g., thresholds on background noise)? None.

Classification.

Target classification will be based on a library-matching procedure, wherein we compare the quality of an unconstrained dipole inversion of the EM61HH-MK2 data with the quality of a dipole fit constrained by principal axis polarizabilities drawn from the signature library. The library values will be based on the mean of the log of the best unconstrained fits from the training data. Fit quality is the squared correlation coefficient between the model fit and the data. If the ratio of the constrained fit quality to the unconstrained fit quality (ρ) is one, then the library item is as good a match to the data as possible. If the ratio is small, then the library item is a poor match.

a. What algorithm is used for discrimination (e.g., multilayer perception, support vector machine)? Rules based.

b. Why is this algorithm used and not others? Past experience.

c. Which parameters are considered possible inputs to the algorithm? Decisions that incorporate the fit ratio, polarizability coefficients, signal amplitude, and fit error will be used to make the final classification decision. The thresholds will be decided by inspection of the above parameters calculated from the training data.

d. What are the outputs of the algorithm (probabilities, confidence levels)? Confidence levels based on separation from unknown source to UXO library.

e. How is the threshold set to decide where the munitions/non-munitions line lies in the discrimination process? Based on training data.

Training.

As part of this demonstration and under previous projects, we have collected in-air data for many of the standard APG ordnance targets. SAIC will collect additional in-air training data for any ordnance not already in our library. The combination of these data will be used for the fit library entries. Many of the targets are composites of two or more distinct parts, for instance, a steel body combined with an aluminum tail assembly. Depending on the distance between the sensors and the target, such items can exhibit a range of slightly different EMI signatures corresponding to excitation from different directions. SAIC will include measurements with the target oriented nose up, nose down, flat, and oblique relative to the sensor.

Our experience at our Blossom Point test site has been that polarizabilities determined from in-air measurements are indistinguishable from those determined from measurements taken over buried targets. SAIC will use data from the calibration lanes, which contain several instances of each target, to establish that this holds true at APG.

SAIC will use target features for clutter items found in the calibration grid. Unfortunately, there are only eight clutter items in the calibration grid, so we will augment our clutter library with features derived from previous surveys over APG. In particular, SAIC will use the results from the ESTCP project 200108, which demonstrated the discrimination capabilities of the EM61HH-MK2 over the blind grid.

a. Which tunable parameters have final values that are optimized over a training set of data, and which have values that are set according to geophysical knowledge (i.e., intuition, experience, common sense)? None.

(1) For those tunable parameters with final values set according to geophysical knowledge:

(a) What is the reasoning behind choosing these particular values? NA.

(b) Why were the final values not optimized over a training set of data? NA.

(2) For those tunable parameters with final values optimized over the training set data:

(a) What training data are used (e.g., all data, a randomly chosen portion of data)? All data.

(b) What error metric is minimized during training (e.g., mean squared error)? Mean squared error between the modeled and measured data.

(c) What learning rule is used during training (e.g., gradient descent)? NA.

(d) What criterion is used to stop training (e.g. number of iterations exceeds threshold, good generalization over validation set of data, ect)? Number of objects included in the training set.

(e) Are all tunable parameters optimized at once or in sequence (in sequence = parameter 1 is held constant at some common sense values while parameter 2 is optimized, then parameter 2 is held constant at its optimized value while parameter 1 is optimized)? NA.

b. What are the final values of all tunable parameters for the characterization process? NA.

2.1.4 Data Submission Format

Data were submitted for scoring in accordance with data submission protocols outlined on the USAEC Web site www.uxotestsites.org. These submitted data are not included in this report in order to protect GT information.

2.1.5 Demonstrator Quality Assurance (QA) and Quality Control (QC) (provided by demonstrator)

Overview of Quality Assurance (QA). At the end of each 1-hour survey session, all survey data are transferred to the field data analyst for preliminary data quality checks. Next, the sensor file is examined for completeness and consistency. At this stage, any sensor malfunctions, drifts, etc., are flagged and reported to the field crew for correction.

Two items need to be checked daily to ensure adequate system performance: geophysical sensor response and reliability of spatial positions measurements. Before beginning survey work each day, the performance of the sensor is measured (after a 10- to 15-minute warm-up) by presenting a standard target to the sensor. The resulting signal is checked against standard values.

Overview of Quality Control (QC). All QC checks and processing will be done using a set of IDL routines that were developed and refined on data from several past surveys. The initial QC checks consist of reading the data files, splitting them into grids, verifying that each grid has the correct number of marked data segments (36 grid points plus starting and ending background), and making raster plots of the data. Additional QC checks and processing will be done using routines that extract the background and grid point readings identified by event marks, allow display and editing of the data, and characterize the anomaly. The anomalies will be characterized by inverting the data to a dipole model each day, in order to monitor the fit quality, which is a measure of how accurately the modeled data matches the measured data. SAIC has seen in past surveys that the fit quality decreases when measurement errors increase. The most common measurement error is positional error caused by the field crew not ensuring the crosshairs on the guide are aligned with the gridlines on the template.

As with the grid template data, the SAINT data will be checked by monitoring the fit quality output from the inversion algorithms. The fit quality decreases with both low SNR signals and with poor positioning. Any anomalies with strong SNR signal but poor fit qualities will be further scrutinized. Any data set which has been deemed unsatisfactory by the data analyst is flagged and not processed further. The anomaly corresponding to the flagged data will be logged for future re-acquisition.

2.1.6 Additional Records

The following record(s) by this vendor can be accessed via the Internet as Microsoft Word documents at www.uxotestsites.org.

2.2 APG SITE INFORMATION

2.2.1 Location

The APG Standardized Test Site is located within a secured range area of the Aberdeen Area. The Aberdeen Area of APG is located approximately 30 miles northeast of Baltimore at the northern end of the Chesapeake Bay. The Standardized Test Site encompasses 17 acres of upland and lowland flats, woods, and wetlands.

2.2.2 Soil Type

According to the soils survey conducted for the entire area of APG in 1998, the test site consists primarily of Elkton Series type soil (ref 2). The Elkton Series consist of very deep, slowly permeable, poorly drained soils. These soils formed in silty aeolin sediments and the underlying loamy alluvial and marine sediments. They are on upland and lowland flats and in depressions of the Mid-Atlantic Coastal Plain. Slopes range from 0 to 2 percent.

ERDC conducted a site-specific analysis in May 2002 (ref 3). The results basically matched the soil survey mentioned above. Seventy percent of the samples taken were classified as silty loam. The majority (77 percent) of the soil samples had a measured water content between 15 and 30 percent with the water content decreasing slightly with depth.

For more details concerning the soil properties at the APG test site, go to www.uxotestsites.org on the Web to view the entire soils description report.

2.2.3 Test Areas

A description of the test site areas at APG is presented in Table 1. A test site layout is shown in Figure 2.

TABLE 1. TEST SITE AREAS

Area	Description
Calibration lanes	Contains 14 standard munitions items buried in six positions, with representation of clutter, at various angles and depths to allow demonstrators to calibrate their equipment.
Blind grid	Contains 400 grid cells in a 0.5-acre site. The center of each grid cell contains either munitions, clutter, or nothing.
Open field	A 10-acre site composed of generally open and flat terrain with minimal clutter and minor navigational obstacles. Vegetation height varies from 15 to 25 cm. This area is subdivided into four subareas (legacy, direct fire, indirect fire, and challenge).
	<ul style="list-style-type: none"> • <i>Open field (legacy)</i> The legacy subarea contains the same wide variety of randomly-placed munitions that were present in the open field prior to the January 2008 general reconfiguration of the site.
	<ul style="list-style-type: none"> • <i>Open field (direct fire)</i> The direct fire subarea contains only three munition types that could be typically found at an impact area of a direct fire weapons range. Munitions and clutter are placed in a pattern typical for these munitions.
	<ul style="list-style-type: none"> • <i>Open field (indirect fire)</i> The indirect fire subarea contains only three munition types that could be typically found at an impact area of an indirect fire weapons range. Munitions and clutter are placed in a pattern typical for these munitions.
	<ul style="list-style-type: none"> • <i>Open field (challenge)</i> The challenge subarea is easily reconfigurable to meet the specific needs and requirements of the demonstrator or the program sponsor. Any results from this area are not reported in the standardized scoring record.
Woods	1.34-acre area consisting of cleared woods (tree removal with only stumps remaining), partially cleared woods (including all underbrush and fallen trees), and virgin woods (i.e., woods in natural state with all trees, underbrush, and fallen trees left in place).
Moguls	1.30-acre area consisting of two areas (the rectangular or driving portion of the course and the triangular section with more difficult, nondrivable terrain). A series of craters (as deep as 0.91 m) and mounds (as high as 0.91 m) encompass this section.

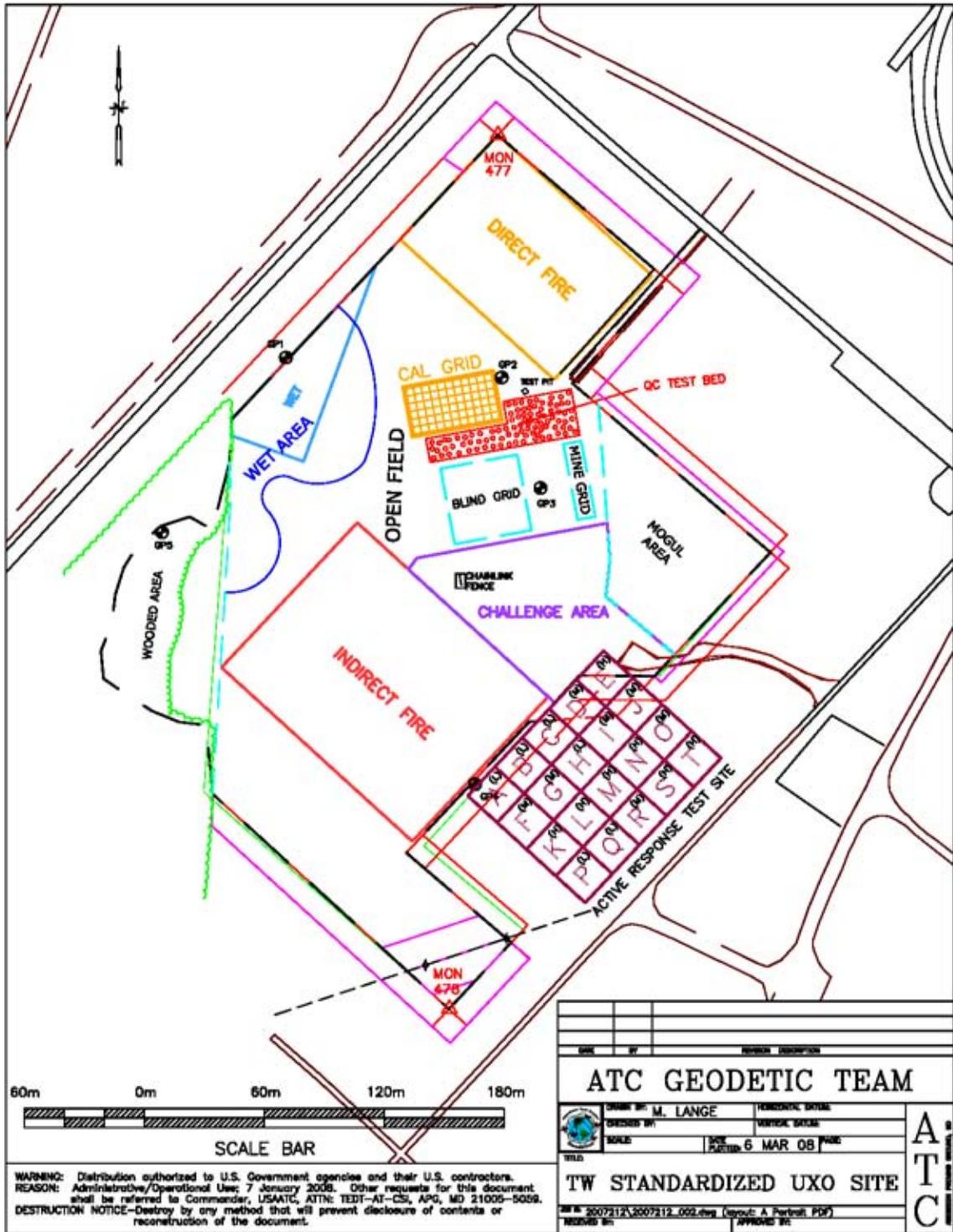


Figure 2. Test site layout.

2.2.4 STANDARD AND NONSTANDARD INERT MUNITIONS TARGETS

The standard and nonstandard munitions items emplaced in the test areas are presented in Table 2. Standardized targets are members of a set of specific munitions items that have identical properties to all other items in the set (caliber, configuration, size, weight, aspect ratio, material, filler, magnetic remanence, and nomenclature). Nonstandard targets are inert munitions items having properties that differ from those in the set of standardized items.

TABLE 2. INERT MUNITIONS TARGETS

Item	Munition Type	Calibration Lanes	Blind Grid	Open Field Direct Fire	Open Field Indirect Fire	Open Field Legacy	Moguls	Woods
20-mm Projectile M55	S	X				X	X	X
25-mm Projectile M794	S	X	X	X				
37-mm Projectile M47	S	X	X	X				
40-mm Projectile MKII Bodies	S	X				X	X	X
BDU-28 Submunition	S	X				X	X	X
BLU-26 Submunition	S	X				X	X	X
M42 Submunition	S	X				X	X	X
57-mm Projectile APC M86	S	X				X	X	X
60-mm Mortar M49A3	S	X	X		X			
2.75-in. Rocket M230	S	X				X	X	X
81-mm Mortar M374	S	X	X		X	X	X	X
105-mm HEAT Rounds M456	S					X	X	X
105-mm HEAT Round M490	S	X	X	X				
105-mm Projectile M60	S	X	X		X	X	X	X
155-mm Projectile M483A1	S	X				X	X	X
20-mm Projectile M55	NS					X	X	X
20-mm Projectile M97	NS					X	X	X
40-mm Projectile M813	NS					X	X	X
60-mm Mortar (JPG)	NS					X	X	X
60-mm Mortar M49	NS					X	X	X
2.75-in. Rocket M230	NS					X	X	X
2.75-in. Rocket XM229	NS					X	X	X
81-mm Mortar (JPG)	NS					X	X	X
81-mm Mortar M374	NS					X	X	X
105-mm Projectile M60	NS					X	X	X
155-mm Projectile M483A	NS					X	X	X

HEAT = high-explosive antitank.
 JPG = Jefferson Proving Ground.
 NS = Nonstandard munition.
 S = Standard munition.

2.3 ATC SURVEY COMMENTS

None.

SECTION 3. FIELD DATA

3.1 DATE OF FIELD ACTIVITIES (22 through 26, and 29 June, 8 and 9 July 2009)

3.2 AREAS TESTED/NUMBER OF HOURS

Areas tested and total numbers of hours operated at each site are presented in Table 3.

TABLE 3. AREAS TESTED AND NUMBER OF HOURS

Area	Number of Hours
Calibration lanes	10.92
Blind grid	36.08
Open field	NA
Woods	NA
Mogul	NA
Mine grid	NA

Note: Table 3 represents the total time spent in each area.

3.3 TEST CONDITIONS

3.3.1 Weather Conditions

An APG weather station located approximately 1 mile west of the test site was used to record average temperature and precipitation on a half-hour basis for each day of operation. The temperatures presented in Table 4 represent the average temperature during field operations from 0700 to 1700 hours, while precipitation data represent a daily total amount of rainfall. Hourly weather logs used to generate this summary are provided in Appendix B.

TABLE 4. TEMPERATURE/PRECIPITATION DATA SUMMARY

Date, 09	Average Temperature, °F	Total Daily Precipitation, in.
22 June	79.4	0.00
23 June	76.7	0.00
24 June	79.9	0.00
25 June	80.8	0.00
26 June	81.8	0.00
29 June	79.5	0.00
8 July	74.3	0.00
9 July	74.8	0.00

3.3.2 Field Conditions

SAIC surveyed the calibration grid and blind grid areas. The field was mainly dry due to conditions prior to and during testing.

3.3.3 Soil Moisture

Three soil probes were placed at various locations within the site to capture soil moisture data: blind grid, calibration, open field, and wooded areas. Measurements were collected in percent moisture and were taken twice daily (morning and afternoon) from five different soil depths (1 to 6 in., 6 to 12 in., 12 to 24 in., 24 to 36 in., and 36 to 48 in.) from each probe. Soil moisture logs are provided in Appendix C.

3.4 FIELD ACTIVITIES

3.4.1 Setup/Mobilization

These activities included initial mobilization and daily equipment preparation and breakdown. A three-person crew took 1 hour and 45 minutes to perform the initial setup and mobilization. A total of 1 hour 55 minutes of equipment preparation was accrued, and end of day equipment breakdown totaled 2 hours and 5 minutes.

3.4.2 Calibration

SAIC spent a total of 10 hours and 55 minutes in the calibration lanes, of which 7 hours was spent collecting data.

3.4.3 Downtime Occasions

Occasions of downtime are grouped into five categories: equipment/data checks or equipment maintenance, equipment failure and repair, weather, demonstration site issues, or breaks/lunch. All downtime is included for the purposes of calculating labor requirements (section 5) except for downtime due to demonstration site issues. Demonstration site issues, while noted in the daily log, are considered nonchargeable downtime for the purposes of calculating labor costs and are not discussed. Breaks and lunches are discussed in this section and billed to the total site survey area.

3.4.3.1 Equipment/data checks, maintenance. Equipment data checks and maintenance activities accounted for 2 hours and 15 minutes of site usage time. These activities included changing out batteries and performing routine data checks to ensure the data were being properly recorded/collected. SAIC spent 1 hour and 45 minutes for breaks and lunches.

3.4.3.2 Equipment failure or repair. A brief equipment failure occurred during this survey. A cable was determined to be loose and was immediately fixed. Downtime for this failure was 15 minutes.

3.4.3.3 Weather. No weather delays occurred during the survey.

3.4.4 Data Collection

**TABLE 5. TOTAL TIME
SAIC, SPENT PER AREA**

Area	Time, hr/min
Blind grid	27 hours, 50 minutes
Open field	NA
Legacy	NA
Direct fire	NA
Indirect fire	NA
Challenge	NA
Wooded	NA
Mine Grid	NA
Moguls	NA

Note: Table 5 represents the total time spent in each area collecting data.

3.4.5 Demobilization

The SAIC survey crew conducted a demonstration of the calibration grid and blind grid. Demobilization occurred on 9 July 2009. On that day, it took the crew 1 hour and 5 minutes to break down and pack up their equipment.

3.5 PROCESSING TIME

SAIC submitted the raw data from the demonstration activities on the last day of the demonstration, as required. The scoring submittal data were provided in December 2009.

3.6 DEMONSTRATOR'S FIELD PERSONNEL

Bruce Barrow (SAIC)
Ivy Carpenter (NAEVA)
Kenneth Robinson (NAEVA)

3.7 DEMONSTRATOR'S FIELD SURVEYING METHOD

SAIC collected the data on a point to point basis. All calibration and blind grid points were surveyed in prior to testing.

3.8 SUMMARY OF DAILY LOGS

Daily logs capture all field activities during this demonstration and are provided in Appendix D.

SECTION 4. TECHNICAL PERFORMANCE RESULTS

4.1 ROC CURVES USING ALL MUNITIONS CATEGORIES

The probability of detection for the response stage (P_d^{res}) and the discrimination stage (P_d^{disc}) versus their respective probability of clutter detection or probability of false positive within each area are shown in Figures 3 through 8. The probabilities plotted against their respective background alarm rate within each area are shown in Figures 9 through 14. Both figures use horizontal lines to illustrate the performance of the demonstrator at two demonstrator-specified points: at the system noise level for the response stage, representing the point below which targets are not considered detectable, and at the demonstrator's recommended threshold level for the discrimination stage, defining the subset of targets the demonstrator would recommend digging based on discrimination. Note that all points have been rounded to protect the GT.

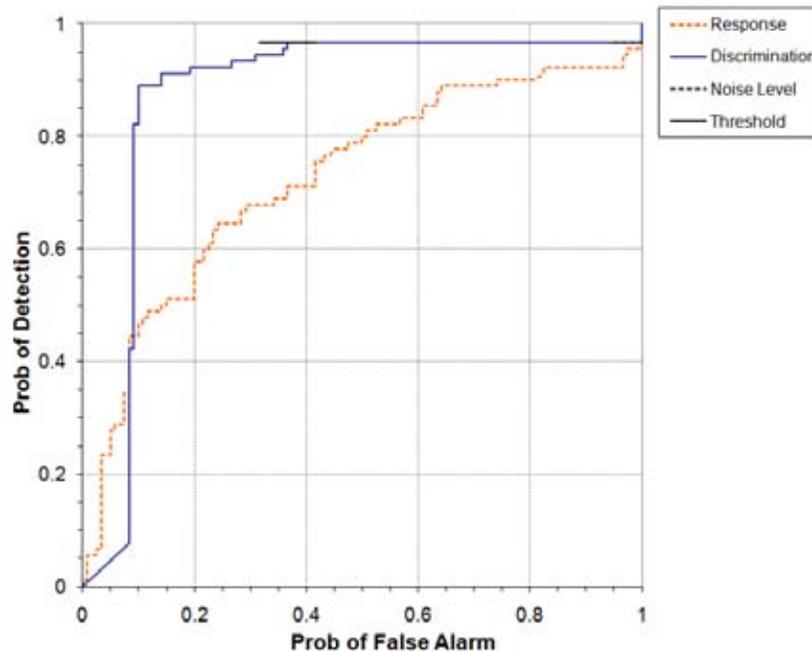


Figure 3. Saint/hand held blind grid probability of detection for response and discrimination stages versus their respective probability of false positive.

Not reported

Figure 4. Saint/hand held open field (direct-fire) probability of detection for response and discrimination stages versus their respective probability of false positive.

Figure 5. Saint/hand held open field (indirect-fire) probability of detection for response and discrimination stages versus their respective probability of false positive.

Not reported

Figure 6. Saint/hand held open field (legacy) probability of detection for response and discrimination stages versus their respective probability of false positive.

Not covered

Figure 7. Saint/hand held wooded probability of detection for response and discrimination stages versus their respective probability of false positive.

Not covered

Figure 8. Saint/hand held mogul probability of detection for response and discrimination stages versus their respective probability of false positive.

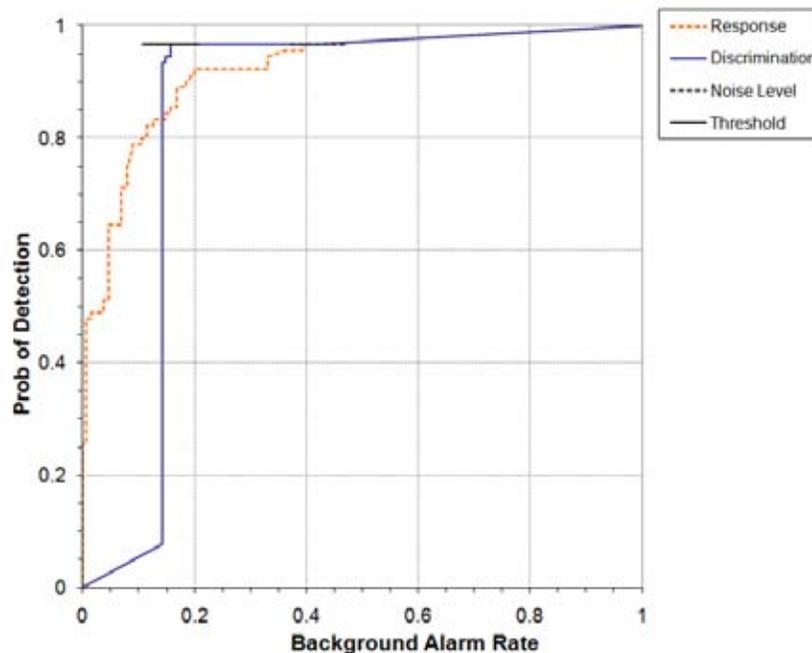


Figure 9. Saint/hand held blind grid probability of detection for response and discrimination stages versus their respective probability of background alarm.

Not reported

Figure 10. Saint/hand held open field (direct fire) probability of detection for response and discrimination stages versus their respective background alarm rate.

Figure 11. Saint/hand held open field (indirect fire) probability of detection for response and discrimination stages versus their respective background alarm rate.

Not reported

Figure 12. Saint/hand held open field (legacy) probability of detection for response and discrimination stages versus their respective background alarm rate.

Not covered

Figure 13. Saint/hand held wooded probability of detection for response and discrimination stages versus their respective background alarm rate.

Not covered

Figure 14. Saint/hand held mogul probability of detection for response and discrimination stages versus their respective background alarm rate.

4.2 PERFORMANCE SUMMARIES

Results for each of the testing areas are presented in Tables 6a through 6f (for labor requirements, see section 5). The response stage results are derived from the list of anomalies above the demonstrator-provided noise level. The results for the discrimination stage are derived from the demonstrator's recommended threshold for optimizing munitions related cleanup by minimizing false alarm digs and maximizing munitions recovery. The lower and upper 90 percent confidence limits on P_d , P_{cd} , and P_{fp} were calculated assuming that the number of detections and false positives are binomially distributed random variables. All results presented in Tables 6a through 6f have been rounded to protect the GT. However, lower confidence limits were calculated using actual results.

TABLE 6a. BLIND GRID TEST AREA RESULTS

Response Stage					Discrimination Stage			
^a Munitions Scores	P_d^{res} : by type				P_d^{disc} : by type			
	All Types	105-mm	81/60-mm	37/25-mm	All Types	105-mm	81/60-mm	37/25-mm
	0.99	0.98	1.00	1.00	0.99	0.98	1.00	1.00
0.97	0.93	0.97	1.00	0.97	0.93	0.97	1.00	
0.93	0.83	0.88	0.93	0.93	0.83	0.88	0.93	
^b By Depth								
0 to 4D	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00
4D to 8D	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00
8D to 12D	0.67	0.67	0.00	1.00	0.67	0.67	0.00	1.00
Clutter Scores	P_{cd}				P_{fp}			
By Mass								
^b By Depth	All Mass	0 to 0.25 kg	>0.25 to 1 kg	>1 to 10 kg	All Mass	0 to 0.25 kg	>0.25 to 1 kg	>1 to 10 kg
All Depth	1.00				0.43			
	1.00	1.00	1.00	1.00	0.37	0.16	0.52	0.80
	0.98				0.31			
0 to 0.15 m	1.00	1.00	1.00	1.00	0.35	0.13	0.53	0.83
0.15 to 0.3 m	1.00	1.00	1.00	1.00	0.50	0.40	0.43	0.75
0.3 to 0.6 m	N/A	N/A	N/A	N/A	N/A	N/A	N/A	N/A
Background Alarm Rates								
	P_{ba}^{res} : 0.42				P_{ba}^{disc} : 0.16			

^aIn cells with offset data entries, the numbers to the left are the result and the two numbers to the right are an upper and lower 90-percent confidence interval for an assumed binomial distribution.

^bAll depths are measured to the center of the object.

TABLE 6b. OPEN FIELD DIRECT FIRE TEST AREA RESULTS (not reported)

Response Stage					Discrimination Stage			
^a Munitions Scores	P_d^{res} : by type				P_d^{disc} : by type			
	All Types	105-mm	37-mm	25-mm	All Types	105-mm	37-mm	25-mm
	--	--	--	--	--	--	--	--
	--	--	--	--	--	--	--	--
<i>By Density</i>								
High	--	--	--	--	--	--	--	--
Medium	--	--	--	--	--	--	--	--
Low	--	--	--	--	--	--	--	--
<i>By Depth^b</i>								
0 to 4D	--	--	--	--	--	--	--	--
4D to 8D	--	--	--	--	--	--	--	--
8D to 12D	--	--	--	--	--	--	--	--
Clutter Scores	P_{cd}				P_{fp}			
<i>By Mass</i>								
^b By Depth	All Mass	0 to 0.25 kg	>0.25 to 1 kg	>1 to 10 kg	All Mass	0 to 0.25 kg	>0.25 to 1 kg	>1 to 10 kg
All Depth	--	--	--	--	--	--	--	--
	--	--	--	--	--	--	--	--
0 to 0.15 m	--	--	--	--	--	--	--	--
0.15 to 0.3 m	--	--	--	--	--	--	--	--
0.3 to 0.6 m	--	--	--	--	--	--	--	--
Background Alarm Rates								
BAR^{res} : --					BAR^{disc} : --			
Groups								
Found	--				--			
Identified	--				--			
Coverage	--				--			

^aIn cells with offset data entries, the numbers to the left are the result and the two numbers to the right are an upper and lower 90-percent confidence interval for an assumed binomial distribution.

^bAll depths are measured to the center of the object.

TABLE 6c. OPEN FIELD INDIRECT FIRE TEST AREA RESULTS

Response Stage					Discrimination Stage			
^a Munitions Scores	P_d^{res} : by type				P_d^{disc} : by type			
	All Types	105-mm	81-mm	60-mm	All Types	105-mm	81-mm	60-mm
	--	--	--	--	--	--	--	--
	--	--	--	--	--	--	--	--
<i>By Density</i>								
High	--	--	--	--	--	--	--	--
Medium	--	--	--	--	--	--	--	--
Low	--	--	--	--	--	--	--	--
<i>By Depth^b</i>								
0 to 4D	--	--	--	--	--	--	--	--
4D to 8D	--	--	--	--	--	--	--	--
8D to 12D	--	--	--	--	--	--	--	--
Clutter Scores	P_{cd}				P_{fp}			
<i>By Mass</i>								
^b By Depth	All Mass	0 to 0.25 kg	>0.25 to 1 kg	>1 to 10 kg	All Mass	0 to 0.25 kg	>0.25 to 1 kg	>1 to 10 kg
All Depth	--	--	--	--	--	--	--	--
	--	--	--	--	--	--	--	--
0 to 0.15 m	--	--	--	--	--	--	--	--
0.15 to 0.3 m	--	--	--	--	--	--	--	--
0.3 to 0.6 m	--	--	--	--	--	--	--	--
Background Alarm Rates								
BAR^{res}:					BAR^{disc}:			
Groups								
Found	--				--			
Identified	--				--			
Coverage	--				--			

^aIn cells with offset data entries, the numbers to the left are the result and the two numbers to the right are an upper and lower 90-percent confidence interval for an assumed binomial distribution.

^bAll depths are measured to the center of the object.

TABLE 6d. OPEN FIELD LEGACY TEST AREA RESULTS (not reported)

Response Stage					Discrimination Stage					
^a Munitions Scores	P_d^{res} : by type				P_d^{disc} : by type					
	All Types	Small	Medium	Large	All Types	Small	Medium	Large		
	--	--	--	--	--	--	--	--	--	
	--	--	--	--	--	--	--	--		
<i>By Depth^b</i>										
0 to 4D	--	--	--	--	--	--	--	--	--	
4D to 8D	--	--	--	--	--	--	--	--	--	
8D to 12D	--	--	--	--	--	--	--	--	--	
> 12D	--	--	--	--	--	--	--	--	--	
Clutter Scores	P_{cd}				P_{fp}					
<i>By Mass</i>										
^b By Depth	All Mass	0 to 0.25 kg	>0.25 to 1 kg	>1 to 10 kg	> 10 kg	All Mass	0 to 0.25 kg	>0.25 to 1 kg	>1 to 8 kg	< 10kg
All Depth	--	--	--	--	--	--	--	--	--	--
0 to 0.15 m	--	--	--	--	--	--	--	--	--	--
0.15 to 0.3 m	--	--	--	--	--	--	--	--	--	--
0.3 to 0.6 m	--	--	--	--	--	--	--	--	--	--
> 0.6 m	--	--	--	--	--	--	--	--	--	--
Background Alarm Rates										
BAR^{res} : --					BAR^{disc} : --					
Groups										
Found	--					--				
Identified	--					--				
Coverage	--					--				

^aIn cells with offset data entries, the numbers to the left are the result and the two numbers to the right are an upper and lower 90-percent confidence interval for an assumed binomial distribution.

^bAll depths are measured to the center of the object.

TABLE 6e. WOODED TEST AREA RESULTS (not covered)

Response Stage					Discrimination Stage					
Munitions Scores	P_d^{res} : by type				P_d^{disc} : by type					
	All Types	Small	Medium	Large	All Types	Small	Medium	Large		
	--	--	--	--	--	--	--	--	--	
	--	--	--	--	--	--	--	--		
<i>By Depth^b</i>										
0 to 4D	--	--	--	--	--	--	--	--		
4D to 8D	--	--	--	--	--	--	--	--		
8D to 12D	--	--	--	--	--	--	--	--		
> 12D	--	--	--	--	--	--	--	--		
Clutter Scores	P_{cd}				P_{fp}					
<i>By Mass</i>										
^b By Depth	All Mass	0 to 0.25 kg	>0.25 to 1 kg	>1 to 10 kg	> 10 kg	All Mass	0 to 0.25 kg	>0.25 to 1 kg	>1 to 8 kg	< 10kg
All Depth	--	--	--	--	--	--	--	--	--	--
0 to 0.15 m	--	--	--	--	--	--	--	--	--	--
0.15 to 0.3 m	--	--	--	--	--	--	--	--	--	--
0.3 to 0.6 m	--	--	--	--	--	--	--	--	--	--
> 0.6 m	--	--	--	--	--	--	--	--	--	--
Background Alarm Rates										
BAR^{res} : --					BAR^{disc} : --					
Groups										
Found	--					--				
Identified	--					--				
Coverage	--					--				

^aIn cells with offset data entries, the numbers to the left are the result and the two numbers to the right are an upper and lower 90-percent confidence interval for an assumed binomial distribution.

^bAll depths are measured to the center of the object.

TABLE 6f. MOGUL TEST AREA RESULTS (not covered)

Response Stage					Discrimination Stage					
^a Munitions Scores	P_d^{res} : by type				P_d^{disc} : by type					
	All Types	Small	Medium	Large	All Types	Small	Medium	Large		
	--	--	--	--	--	--	--	--	--	
<i>By Depth^b</i>										
0 to 4D	--	--	--	--	--	--	--	--	--	
4D to 8D	--	--	--	--	--	--	--	--	--	
8D to 12D	--	--	--	--	--	--	--	--	--	
> 12D	--	--	--	--	--	--	--	--	--	
Clutter Scores	P_{cd}				P_{fp}					
<i>By Mass</i>										
^b By Depth	All Mass	0 to 0.25 kg	>0.25 to 1 kg	>1 to 10 kg	> 10 kg	All Mass	0 to 0.25 kg	>0.25 to 1 kg	>1 to 8 kg	< 10kg
All Depth	--	--	--	--	--	--	--	--	--	--
0 to 0.15 m	--	--	--	--	--	--	--	--	--	--
0.15 to 0.3 m	--	--	--	--	--	--	--	--	--	--
0.3 to 0.6 m	--	--	--	--	--	--	--	--	--	--
> 0.6 m	--	--	--	--	--	--	--	--	--	--
Background Alarm Rates										
BAR^{res} : --					BAR^{disc} : --					
Groups										
Found	--					--				
Identified	--					--				
Coverage	--					--				

^aIn cells with offset data entries, the numbers to the left are the result and the two numbers to the right are an upper and lower 90-percent confidence interval for an assumed binomial distribution.

^bAll depths are measured to the center of the object.

4.3 EFFICIENCY, REJECTION RATES, AND TYPE CLASSIFICATION

Efficiency and rejection rates are calculated to quantify the discrimination ability at specific points of interest on the ROC curve: one at the point where no decrease in P_d is suffered (i.e., the efficiency is by definition equal to one) and the other at the operator selected threshold. These values are presented in Tables 7a through 7f.

TABLE 7a. BLIND GRID EFFICIENCY AND REJECTION RATES

	Efficiency (E)	False Positive Rejection Rate	Background Alarm Rejection Rate
At Operating Point	1.00	0.63	0.63
With No Loss of P _d	1.00	0.63	0.63

TABLE 7b. OPEN FIELD (DIRECT) EFFICIENCY AND REJECTION RATES (not reported)

	Efficiency (E)	False Positive Rejection Rate	Background Alarm Rejection Rate
At Operating Point	--	--	--
With No Loss of P _d	--	--	--

TABLE 7c. OPEN FIELD (INDIRECT) EFFICIENCY AND REJECTION RATES

	Efficiency (E)	False Positive Rejection Rate	Background Alarm Rejection Rate
At Operating Point	--	--	--
With No Loss of P _d	--	--	--

TABLE 7d. OPEN FIELD (LEGACY) EFFICIENCY AND REJECTION RATES (not reported)

	Efficiency (E)	False Positive Rejection Rate	Background Alarm Rejection Rate
At Operating Point	--	--	--
With No Loss of P _d	--	--	--

TABLE 7e. WOODED EFFICIENCY AND REJECTION RATES (not covered)

	Efficiency (E)	False Positive Rejection Rate	Background Alarm Rejection Rate
At Operating Point	--	--	--
With No Loss of P _d	--	--	--

TABLE 7f. MOGUL EFFICIENCY AND REJECTION RATES (not covered)

	Efficiency (E)	False Positive Rejection Rate	Background Alarm Rejection Rate
At Operating Point	--	--	--
With No Loss of P _d	--	--	--

At the demonstrator's recommended setting, the munitions items that were detected and correctly discriminated were further scored on whether their correct type could be identified (tables 8a through 8f). Correct type examples include 20-mm projectile, 105-mm HEAT projectile, and 2.75-inch rocket. A list of the standard type declaration required for each munitions item was provided to demonstrators prior to testing. The standard types for the three example items are 20-mmP, 105H, and 2.75-inch.

TABLE 8a. BLIND GRID CORRECT TYPE CLASSIFICATION OF TARGETS CORRECTLY DISCRIMINATED AS MUNITIONS

Size	Percentage
25mm	93
37mm	100
60mm	100
81mm	93
105mm	77
Overall	90

Note: The demonstrator did not attempt to provide separate type classifications for the two different 105mm rounds. They are grouped together for analysis in this table only.

TABLE 8b. OPEN FIELD DIRECT FIRE CORRECT TYPE CLASSIFICATION OF TARGETS CORRECTLY DISCRIMINATED AS MUNITIONS (not reported)

Size	Percentage
25mm	--
37mm	--
105mm	--
Overall	--

**TABLE 8c. OPEN FIELD INDIRECT FIRE
CORRECT TYPE CLASSIFICATION
OF TARGETS CORRECTLY
DISCRIMINATED AS
MUNITIONS**

Size	Percentage
60mm	--
81mm	--
105mm	--
Overall	--

**TABLE 8d. OPEN FIELD LEGACY CORRECT
TYPE CLASSIFICATION OF TARGETS
CORRECTLY DISCRIMINATED
AS MUNITIONS (not reported)**

Size	Percentage
Small	--
Medium	--
Large	--
Overall	--

**TABLE 8e. WOODED CORRECT TYPE
CLASSIFICATION OF TARGETS
CORRECTLY DISCRIMINATED
AS MUNITIONS (not covered)**

Size	Percentage
Small	--
Medium	--
Large	--
Overall	--

**TABLE 8f. MOGUL CORRECT TYPE
CLASSIFICATION OF TARGETS
CORRECTLY DISCRIMINATED
AS MUNITIONS (not covered)**

Size	Percentage
Small	--
Medium	--
Large	--
Overall	--

4.4 LOCATION ACCURACY

The mean location error and standard deviations are presented in Tables 9a through 9f. These calculations are based on average missed distance for munitions correctly identified during the response stage. Depths are measured from the center of the munitions to the surface. For the blind grid, only depth errors are calculated because (X, Y) positions are known to be the centers of the grid square.

**TABLE 9a. BLIND GRID MEAN LOCATION ERROR
AND STANDARD DEVIATION**

	Mean	Standard Deviation
Northing	NA	NA
Easting	NA	NA
Depth	0.122	0.060

**TABLE 9b. OPEN FIELD DIRECT FIRE MEAN
LOCATION ERROR AND
STANDARD DEVIATION (not reported)**

	Mean	Standard Deviation
Northing	--	--
Easting	--	--
Depth	--	--

TABLE 9c. OPEN FIELD INDIRECT FIRE MEAN LOCATION ERROR AND STANDARD DEVIATION

	Mean	Standard Deviation
Northing	--	--
Easting	--	--
Depth	--	--

TABLE 9d. OPEN FIELD LEGACY MEAN LOCATION ERROR AND STANDARD DEVIATION (not reported)

	Mean	Standard Deviation
Northing	--	--
Easting	--	--
Depth	--	--

TABLE 9e. WOODED MEAN LOCATION ERROR AND STANDARD DEVIATION (not covered)

	Mean	Standard Deviation
Northing	--	--
Easting	--	--
Depth	--	--

TABLE 9f. MOGUL MEAN LOCATION ERROR AND STANDARD DEVIATION (not covered)

	Mean	Standard Deviation
Northing	--	--
Easting	--	--
Depth	--	--

SECTION 5. APPENDIXES

APPENDIX A. TERMS AND DEFINITIONS

GENERAL DEFINITIONS

Anomaly: Location of a system response deemed to warrant further investigation by the demonstrator for consideration as an emplaced munitions item.

Detection: An anomaly location that is within R_{halo} of an emplaced munitions item.

Military Munitions (MM): Specific categories of MM that may pose unique explosive safety risks, including UXO as defined in 10 USC 101(e)(5), DMM as defined in 10 USC 2710(e)(2) and/or munitions constituents (e.g., TNT, RDX) as defined in 10 USC 2710(e)(3) that are present in high enough concentrations to pose an explosive hazard.

Emplaced Munitions: A munitions item buried by the government at a specified location in the test site.

Emplaced Clutter: A clutter item (i.e., nonmunitions item) buried by the government at a specified location in the test site.

R_{halo} : A predetermined radius about an emplaced item (clutter or munitions) within which an anomaly identified by the demonstrator as being of interest is considered to be a detection of that item. For the purpose of this program, a circular halo 0.5 meters in radius is placed around the center of the object for all clutter and munitions items.

Small Munitions: Caliber of munitions less than or equal to 40 mm (includes 20-mm projectile, 25-mm projectile, 37-mm projectile, 40-mm projectile, submunitions BLU-26, BLU-63, and M42).

Medium Munitions: Caliber of munitions greater than 40 mm and less than or equal to 81 mm (includes 57-mm projectile, 60-mm mortar, 2.75-inch rocket, and 81-mm mortar).

Large Munitions: Caliber of munitions greater than 81 mm (includes 105-mm HEAT, 105-mm projectile, and 155-mm projectile).

Group: Two or more adjacent GT items with overlapping halos.

GT: Ground truth

Response Stage Noise Level: The level that represents the signal level below which anomalies are not considered detectable. Demonstrators are required to provide the recommended noise level for the blind grid test area.

Discrimination Stage Threshold: The demonstrator-selected threshold level that is expected to provide optimum performance of the system by retaining all detectable munitions and rejecting the maximum amount of clutter. This level defines the subset of anomalies the demonstrator would recommend digging based on discrimination.

Binomially Distributed Random Variable: A random variable of the type which has only two possible outcomes, say success and failure, is repeated for n independent trials with the probability p of success and the probability $1-p$ of failure being the same for each trial. The number of successes x observed in the n trials is an estimate of p and is considered to be a binomially distributed random variable.

RESPONSE AND DISCRIMINATION STAGE DATA

The scoring of the demonstrator's performance is conducted in two stages: response stage and discrimination stage. For both stages, the probability of detection (P_d) and the false alarms are reported as receiver-operating characteristic (ROC) curves. False alarms are divided into those anomalies that correspond to emplaced clutter items, measuring the probability of clutter detection (P_{cd}) or probability of false positive (P_{fp}). Those that do not correspond to any known item are termed background alarms.

The response stage is a measure of whether the sensor can detect an object of interest. For a channel instrument, this value should be closely related to the amplitude of the signal. The demonstrator must report the response level (threshold) below which target responses are deemed insufficient to warrant further investigation. At this stage, minimal processing may be done. This includes filtering long- and short-scale variations, bias removal, and scaling. This processing should be detailed in the data submission.

For a multichannel instrument, the demonstrator must construct a quantity analogous to amplitude. The demonstrator should consider what combination of channels provides the best test for detecting any object that the sensor can detect. The average amplitude across a set of channels is an example of an acceptable response stage quantity. Other methods may be more appropriate for a given sensor. Again, minimal processing can be done, and the demonstrator should explain how this quantity was constructed in their data submission.

The discrimination stage evaluates the demonstrator's ability to correctly identify munitions as such, and to reject clutter. For the same locations as in the response stage anomaly list, the discrimination stage list contains the output of the algorithms applied in the discrimination-stage processing. This list is prioritized based on the demonstrator's determination that an anomaly location is likely to contain munitions. Thus, higher output values are indicative of higher confidence that a munitions item is present at the specified location. For electronic signal processing, priority ranking is based on algorithm output. For other systems, priority ranking is based on human judgment. The demonstrator also selects the threshold that the demonstrator believes will provide optimum system performance, (i.e., that retains all the detected munitions and rejects the maximum amount of clutter).

Note: The two lists provided by the demonstrator contain identical numbers of potential target locations. They differ only in the priority ranking of the declarations.

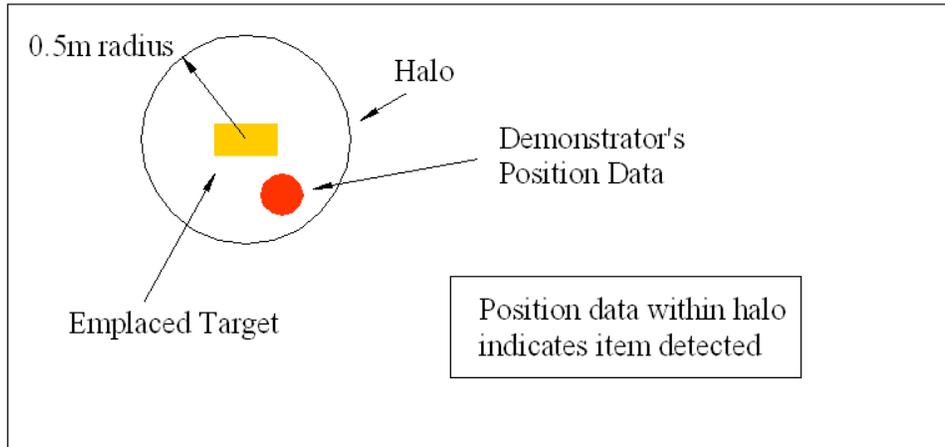
GROUP SCORING FACTORS

Based on configuration of the GT at the standardized sites and the defined scoring methodology, there exists munitions groups defined as having overlapping halos. In these cases, the following scoring logic is implemented (fig. A-1 through A-9):

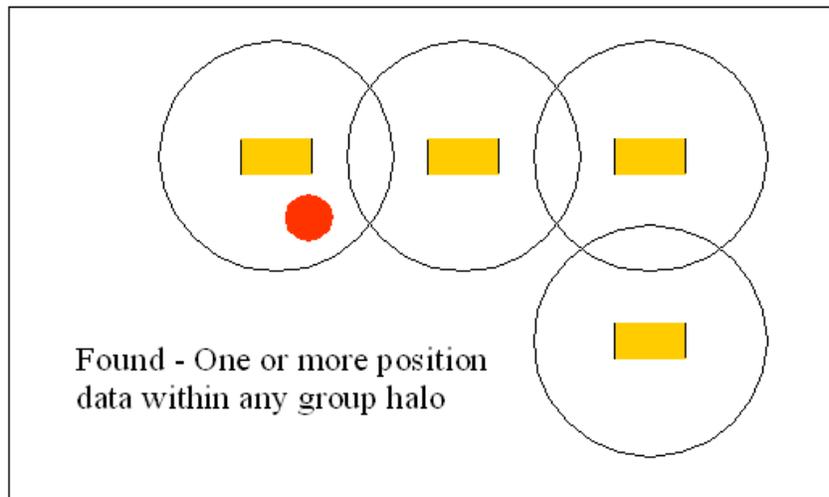
- a. Overall site scores (i.e., P_d) will consider only isolated munitions and clutter items.
- b. GT items that have overlapping halos (both munitions and clutter) will form a group and groups may form chains.
- c. Groups will have a complex halos composed of all the composite halos of all its GT items.
- d. Groups will have three scoring factors: groups found groups identified and group coverage. Scores will be based on 1:1 matches of anomalies and GT.
 - (1) Groups Found (Found): the number of groups that have one or more GT items matched divided by the total number of groups. Demonstrators will be credited with detecting a group if any item within the group is matched to an anomaly in their list.
 - (2) Groups Identified (ID): the number of groups that have two or more GT items matched divided by the total number of groups. Demonstrators will be credited with identifying that a group is present if multiple items within the composite halo are matched to anomalies in their list.
 - (3) Group Coverage (Coverage): the number of GT items matched within groups divided by the total number of GT items within groups. This metric measures the demonstrator accuracy in determining the number of anomalies within a group. If five items are present and only two anomalies are matched, the demonstrator will score 0.4. If all five are matched the demonstrator will score 1.0.
- e. Location error will not be reported for groups.

f. Demonstrators will not be asked to call out groups in their scoring submissions. If multiple anomalies are indicated in a small area, the demonstrator will report all individual anomalies.

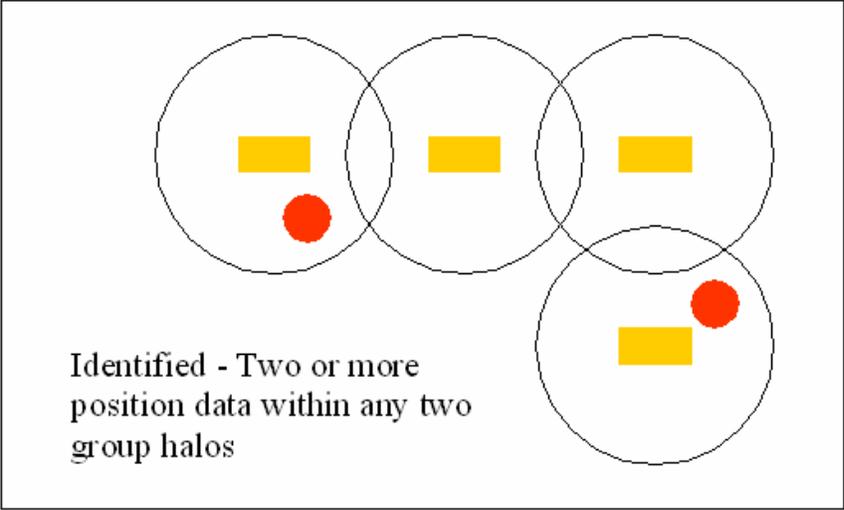
g. Excess alarms within a halo will be disregarded.



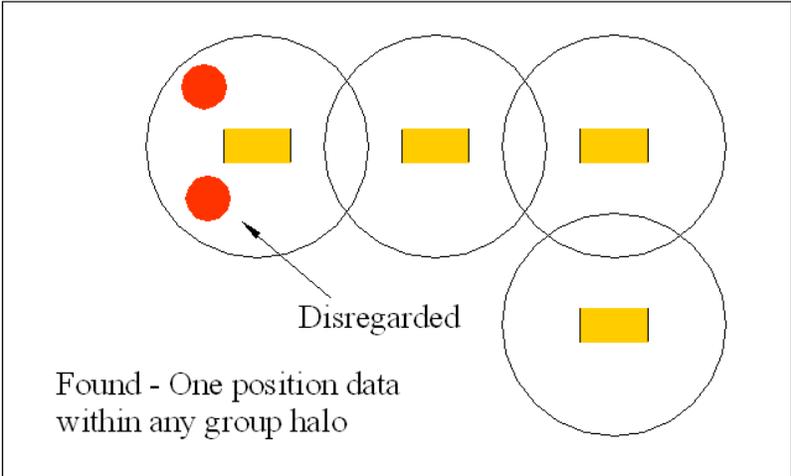
A-1. Example of detected item.



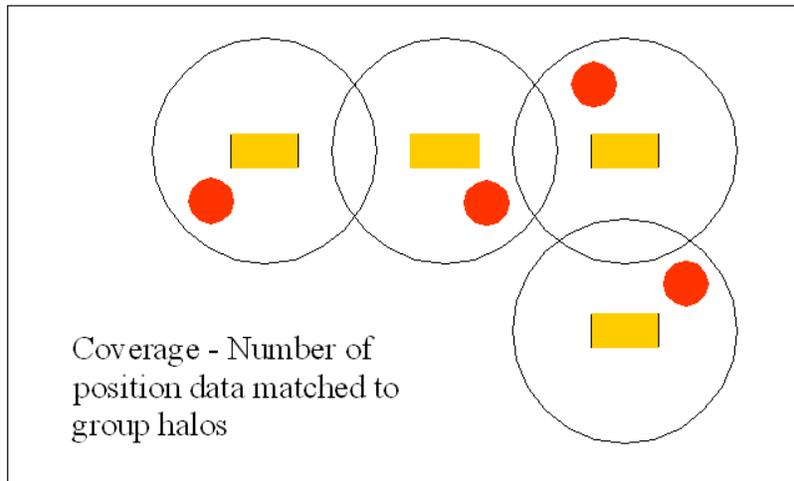
A-2. Example of group found (found).



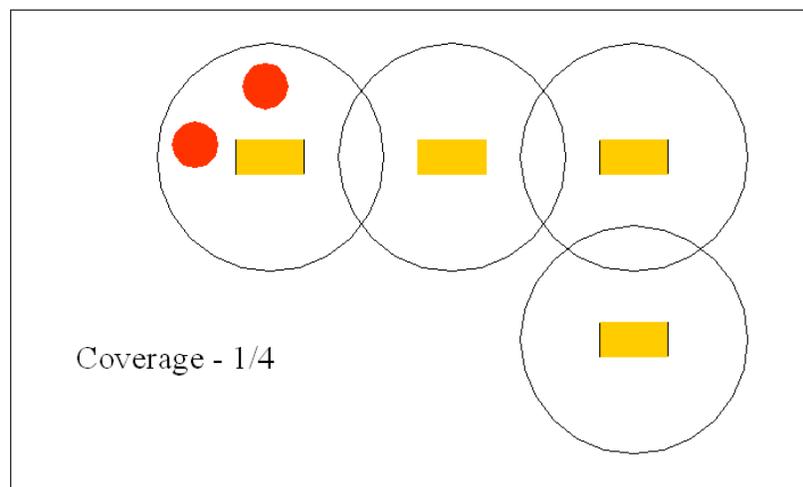
A-3. Example of group identified (ID).



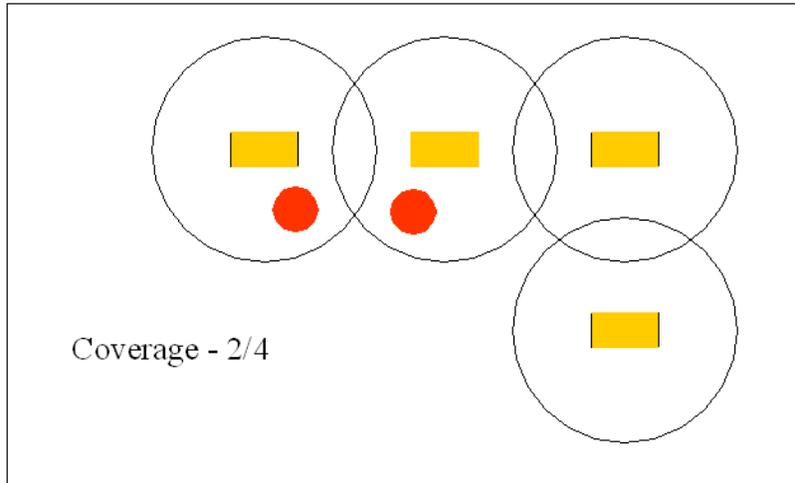
A-4. Example of excess alarms disregarded.



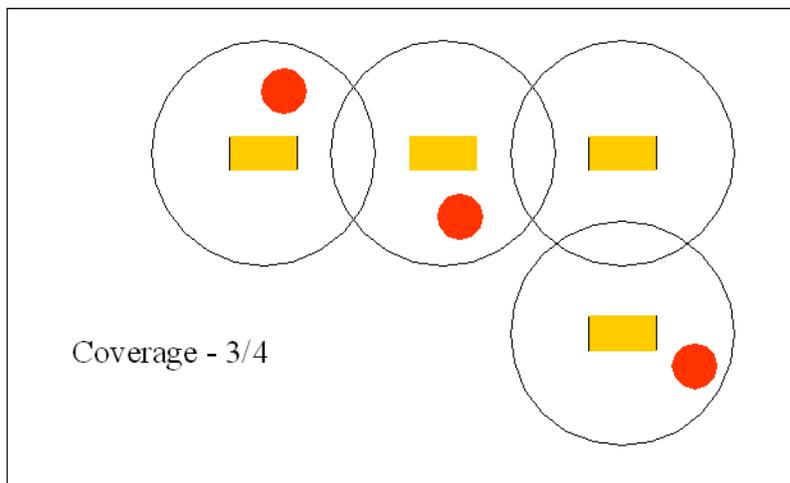
A-5. Example of a group.



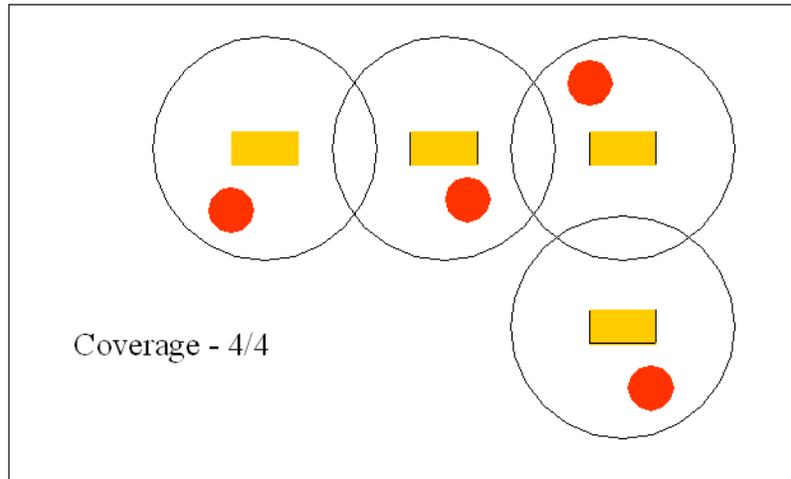
A-6. Example of group ($1/4 = 0.25$).



A-7. Example of group ($2/4 = 0.5$).



A-8. Example of group ($3/4 = 0.75$).



A-9. Example of group ($4/4 = 1.0$).

RESPONSE STAGE DEFINITIONS

Response Stage Probability of Detection (P_d^{res}): $P_d^{\text{res}} = (\text{No. of response-stage detections}) / (\text{No. of emplaced munitions in the test site})$.

Response Stage Clutter Detection (cd^{res}): An anomaly location that is within R_{halo} of an emplaced clutter item.

Response Stage Probability of Clutter Detection (P_{cd}^{res}): $P_{cd}^{\text{res}} = (\text{No. of response-stage clutter detections}) / (\text{No. of emplaced clutter items})$.

Response Stage Background Alarm (ba^{res}): An anomaly in a blind grid cell that contains neither emplaced munitions nor an emplaced clutter item. An anomaly location in the open field or scenarios that is outside R_{halo} of any emplaced munitions or emplaced clutter item.

Response Stage Probability of Background Alarm (P_{ba}^{res}): Blind grid only: $P_{ba}^{\text{res}} = (\text{No. of response-stage background alarms}) / (\text{No. of empty grid locations})$.

Response Stage Background Alarm Rate (BAR^{res}): Open field any challenge area (including the direct and indirect firing sub areas) only: $BAR^{\text{res}} = (\text{No. of response-stage background alarms}) / (\text{arbitrary constant})$.

Note that the quantities P_d^{res} , P_{cd}^{res} , P_{ba}^{res} , and BAR^{res} are functions of t^{res} , the threshold applied to the response-stage signal strength. These quantities can therefore be written as $P_d^{\text{res}}(t^{\text{res}})$, $P_{cd}^{\text{res}}(t^{\text{res}})$, $P_{ba}^{\text{res}}(t^{\text{res}})$, and $BAR^{\text{res}}(t^{\text{res}})$.

DISCRIMINATION STAGE DEFINITIONS

Discrimination: The application of a signal processing algorithm or human judgment to sensor data to discriminate munitions from clutter. Discrimination should identify anomalies that the demonstrator has high confidence correspond to munitions, as well as those that the demonstrator has high confidence correspond to nonmunitions or background returns. The former should be ranked with highest priority and the latter with lowest.

Discrimination Stage Probability of Detection (P_d^{disc}): $P_d^{\text{disc}} = (\text{No. of discrimination-stage detections})/(\text{No. of emplaced munitions in the test site})$.

Discrimination Stage False Positive (fp^{disc}): An anomaly location that is within R_{halo} of an emplaced clutter item.

Discrimination Stage Probability of False Positive ($P_{\text{fp}}^{\text{disc}}$): $P_{\text{fp}}^{\text{disc}} = (\text{No. of discrimination stage false positives})/(\text{No. of emplaced clutter items})$.

Discrimination Stage Background Alarm (ba^{disc}): An anomaly in a blind grid cell that contains neither emplaced munitions nor an emplaced clutter item. An anomaly location in the open field or scenarios that is outside R_{halo} of any emplaced munitions or emplaced clutter item.

Discrimination Stage Probability of Background Alarm ($P_{\text{ba}}^{\text{disc}}$): $P_{\text{ba}}^{\text{disc}} = (\text{No. of discrimination-stage background alarms})/(\text{No. of empty grid locations})$.

Discrimination Stage Background Alarm Rate (BAR^{disc}): $\text{BAR}^{\text{disc}} = (\text{No. of discrimination-stage background alarms})/(\text{arbitrary constant})$.

Note that the quantities P_d^{disc} , $P_{\text{fp}}^{\text{disc}}$, $P_{\text{ba}}^{\text{disc}}$, and BAR^{disc} are functions of t^{disc} , the threshold applied to the discrimination-stage signal strength. These quantities can therefore be written as $P_d^{\text{disc}}(t^{\text{disc}})$, $P_{\text{fp}}^{\text{disc}}(t^{\text{disc}})$, $P_{\text{ba}}^{\text{disc}}(t^{\text{disc}})$, and $\text{BAR}^{\text{disc}}(t^{\text{disc}})$.

RECEIVER-OPERATING CHARACTERISTIC (ROC) CURVES

ROC curves at both the response and discrimination stages can be constructed based on the above definitions. The ROC curves plot the relationship between P_d versus P_{cd} or P_{fp} and P_d versus BAR or P_{ba} as the threshold applied to the signal strength is varied from its minimum (t_{min}) to its maximum (t_{max}) value.¹ P_d versus P_{fp} and P_d versus BAR being combined into ROC curves is shown in Figure A-10. Note that the “res” and “disc” superscripts have been suppressed from all the variables for clarity.

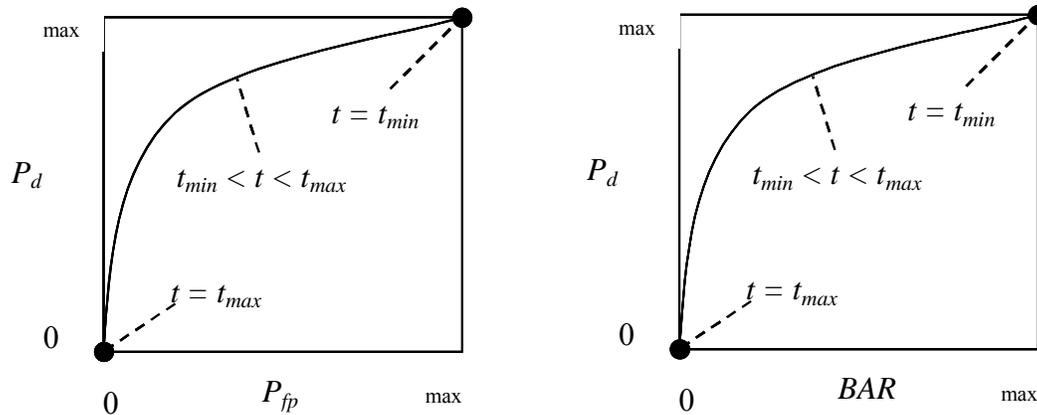


Figure A-10. ROC curves for open field testing. Each curve applies to both the response and discrimination stages.

METRICS TO CHARACTERIZE THE DISCRIMINATION STAGE

The demonstrator is also scored on efficiency and rejection ratio, which measure the effectiveness of the discrimination stage processing. The goal of discrimination is to retain the greatest number of munitions detections from the anomaly list while rejecting the maximum number of anomalies arising from nonmunitions items. The efficiency measures the fraction of detected munitions retained by the discrimination, while the rejection ratio measures the fraction of false alarms rejected. Both measures are defined relative to the entire response list, i.e., the maximum munitions detectable by the sensor and its accompanying clutter detection rate/false positive rate or background alarm rate.

¹Strictly speaking, ROC curves plot the P_d versus P_{ba} over a predetermined and fixed number of detection opportunities (some of the opportunities are located over munitions and others are located over clutter or blank spots). In an open field scenario, each system suppresses its signal strength reports until some bare-minimum signal response is received by the system. Consequently, the open field ROC curves do not have information from low signal-output locations, and, furthermore, different contractors report their signals over a different set of locations on the ground. These ROC curves are thus not true to the strict definition of ROC curves as defined in textbooks on detection theory. Note, however, that the ROC curves obtained in the blind grid test sites are true ROC curves.

Efficiency (E): $E = P_d^{disc}(t^{disc})/P_d^{res}(t_{min}^{res})$: Measures (at a threshold of interest) the degree to which the maximum theoretical detection performance of the sensor system (as determined by the response stage t_{min}) is preserved after application of discrimination techniques. Efficiency is a number between 0 and 1. An efficiency of 1 implies that all of the munitions initially detected in the response stage were retained at the specified threshold in the discrimination stage, t^{disc} .

False Positive Rejection Rate (R_{fp}): $R_{fp} = 1 - [P_{fp}^{disc}(t^{disc})/P_{cd}^{res}(t_{min}^{res})]$: Measures (at a threshold of interest) the degree to which the sensor system's false positive performance is improved over the maximum false positive performance (as determined by the response stage t_{min}). The rejection rate is a number between 0 and 1. A rejection rate of 1 implies that all misplaced clutter initially detected in the response stage were correctly rejected at the specified threshold in the discrimination stage.

Background Alarm Rejection Rate (R_{ba}):

Blind grid: $R_{ba} = 1 - [P_{ba}^{disc}(t^{disc})/P_{ba}^{res}(t_{min}^{res})]$.

Open field: $R_{ba} = 1 - [BAR^{disc}(t^{disc})/BAR^{res}(t_{min}^{res})]$.

Measures the degree to which the discrimination stage correctly rejects background alarms initially detected in the response stage. The rejection rate is a number between 0 and 1. A rejection rate of 1 implies that all background alarms initially detected in the response stage were rejected at the specified threshold in the discrimination stage.

CHI-SQUARE COMPARISON

The Chi-square test for differences in probabilities (or 2 by 2 contingency table) is used to analyze two samples drawn from two different populations to see if both populations have the same or different proportions of elements in a certain category. More specifically, two random samples are drawn, one from each population, to test the null hypothesis that the probability of event A (some specified event) is the same for both populations.

The test statistic of the 2 by 2 contingency table is the Chi-square distribution with one degree of freedom. When an association between a more challenging terrain feature and relatively degraded performance is sought, a one-sided test is performed. A two-sided 2 by 2 contingency table is used in the Standardized UXO Technology Demonstration Site Program to compare performance between any two areas or subareas when the direction of degradation cannot be predetermined.

For a one-sided test, a significance level of 0.05 is used to set the critical decision limit. It is a critical decision limit because if the test statistic calculated from the data exceeds this value, then the lower proportion tested will be considered significantly less than the greater one (degraded). If the test statistic calculated from the data is less than this value, then no degradation can be said to exist because of the terrain feature introduced.

For a two-sided test, a significance level of 0.10 is used to allow .05 on either side of the decision. It is a critical decision limit because if the test statistic calculated from the data exceeds this value, then the two proportions tested will be considered significantly different. If the test statistic calculated from the data is less than this value, then the two proportions tested will be considered not significantly different.

An exception must be applied when either a 0 or 100 percent success rate occurs in the sample data. The Chi-square test cannot be used in these instances. Instead, Fischer's test is used, and the critical decision limit for one-sided tests is the chosen significance level, which in this case is 0.05. With Fischer's test, if the test statistic is less than the critical value, then the proportions are considered to be significantly different.

An example follows that illustrates Standardized UXO Technology Demonstration Site blind grid results compared to those from the open field legacy. It should be noted that a significant result does not prove a cause-and-effect relationship exists between the two populations of interest; however, it does serve as a tool to indicate that one data set has experienced a degradation or change in system performance at a large enough level than can be accounted for merely by chance or random variation. Note also that a result that is not significant indicates that there is not enough evidence to declare that anything more than chance or random variation within the same population is at work between the two data sets being compared.

Demonstrator X achieves the following overall results after surveying the blind grid and open field (legacy) using the same system (results indicate the number of munitions detected divided by the number of munitions emplaced):

	Blind grid		Open field
P_d^{res}	100/100 = 1.0		8/10 = .80

P_d^{res} : BLIND GRID versus OPEN FIELD (legacy). Using the example data above to compare probabilities of detection in the response stage, all 100 munitions out of 100 emplaced munitions items were detected in the blind grid while 8 munitions out of 10 emplaced were detected in the open field. Fischer's test must be used since a 100 percent success rate occurs in the data. Fischer's test uses the four input values to calculate a test statistic of 0.0075 that is compared against the critical value of 0.05. Since the test statistic is less than the critical value, the smaller response stage detection rate (0.80) is considered to be significantly less at the 0.05 level of significance. While a significant result does not prove a cause-and-effect relationship exists between the change in survey area and degradation in performance, it does indicate that the detection ability of demonstrator X's system seems to have been degraded in the open field relative to results from the blind grid using the same system. This is an example of a one-sided Chi-squared test.

APPENDIX B. DAILY WEATHER LOGS

Date, 2009	Time, ^aEST	Avg Temp, °F	Total Precip, in.
22 Jun	7:00	72.0	0.00
	8:00	75.0	0.00
	9:00	77.4	0.00
	10:00	77.5	0.00
	11:00	78.4	0.00
	12:00	80.4	0.00
	13:00	81.5	0.00
	14:00	82.6	0.00
	15:00	82.9	0.00
	16:00	82.6	0.00
	17:00	83.1	0.00
23 Jun	7:00	70.0	0.00
	8:00	71.2	0.00
	9:00	73.8	0.00
	10:00	75.2	0.00
	11:00	75.6	0.00
	12:00	77.2	0.00
	13:00	78.1	0.00
	14:00	79.5	0.00
	15:00	80.6	0.00
	16:00	80.2	0.00
	17:00	82.0	0.00
24 Jun	7:00	71.6	0.00
	8:00	74.3	0.00
	9:00	77.5	0.00
	10:00	79.5	0.00
	11:00	81.5	0.00
	12:00	82.2	0.00
	13:00	81.9	0.00
	14:00	81.9	0.00
	15:00	82.8	0.00
	16:00	83.1	0.00
	17:00	83.7	0.00

^aEastern Standard Time

Date, 2009	Time, ^aEST	Avg Temp, °F	Total Precip, in.
25 Jun	7:00	71.4	0.00
	8:00	73.8	0.00
	9:00	76.3	0.00
	10:00	79.5	0.00
	11:00	81.5	0.00
	12:00	83.5	0.00
	13:00	82.8	0.00
	14:00	84.4	0.00
	15:00	85.8	0.00
	16:00	84.9	0.00
	17:00	84.9	0.00
26 Jun	7:00	72.7	0.00
	8:00	75.2	0.00
	9:00	76.8	0.00
	10:00	79.0	0.00
	11:00	82.8	0.00
	12:00	83.8	0.00
	13:00	85.1	0.00
	14:00	86.9	0.00
	15:00	87.1	0.00
	16:00	86.4	0.00
	17:00	84.4	0.00
29 Jun	7:00	69.4	0.00
	8:00	73.2	0.00
	9:00	76.1	0.00
	10:00	78.3	0.00
	11:00	79.9	0.00
	12:00	81.3	0.00
	13:00	82.4	0.00
	14:00	83.3	0.00
	15:00	83.5	0.00
	16:00	83.5	0.00
	17:00	84.2	0.00

Date, 2009	Time, ^aEST	Avg Temp, °F	Total Precip, in.
30 Jun	7:00	70.2	0.00
	8:00	76.5	0.00
	9:00	79.2	0.00
	10:00	81.0	0.00
	11:00	81.3	0.00
	12:00	82.8	0.00
	13:00	82.9	0.00
	14:00	76.1	0.28
	15:00	69.3	0.00
	16:00	74.7	0.00
	17:00	76.6	0.00
1 Jul	7:00	66.7	0.00
	8:00	69.3	0.00
	9:00	71.4	0.00
	10:00	75.2	0.00
	11:00	77.7	0.00
	12:00	79.3	0.00
	13:00	80.6	0.00
	14:00	81.5	0.00
	15:00	82.8	0.00
	16:00	83.7	0.00
	17:00	82.8	0.00
6 Jul	7:00	66.7	0.00
	8:00	71.6	0.00
	9:00	76.1	0.00
	10:00	78.4	0.00
	11:00	79.5	0.00
	12:00	80.6	0.00
	13:00	81.7	0.00
	14:00	82.4	0.00
	15:00	83.5	0.00
	16:00	84.4	0.00
	17:00	84.7	0.00

Date, 2009	Time, ^aEST	Avg Temp, °F	Total Precip, in.
7 Jul	7:00	69.4	0.00
	8:00	73.8	0.00
	9:00	77.0	0.00
	10:00	80.4	0.00
	11:00	82.0	0.00
	12:00	83.3	0.00
	13:00	83.1	0.00
	14:00	84.7	0.00
	15:00	84.9	0.00
	16:00	85.3	0.00
	17:00	85.3	0.00
8 Jul	7:00	66.4	0.00
	8:00	68.9	0.00
	9:00	71.2	0.00
	10:00	73.2	0.00
	11:00	74.7	0.00
	12:00	75.6	0.00
	13:00	76.1	0.00
	14:00	76.6	0.00
	15:00	77.5	0.00
	16:00	77.9	0.00
	17:00	78.6	0.00
9 Jul	7:00	65.5	0.00
	8:00	69.4	0.00
	9:00	71.1	0.00
	10:00	72.5	0.00
	11:00	74.3	0.00
	12:00	76.3	0.00
	13:00	77.7	0.00
	14:00	78.8	0.00
	15:00	79.0	0.00
	16:00	79.7	0.00
	17:00	79.0	0.00

APPENDIX C. SOIL MOISTURE

Date: 22 Jun 09			
Probe Location	Layer, in.	AM Reading, %	PM Reading, %
Wet area	0 to 6	--	--
	6 to 12	--	--
	12 to 24	--	--
	24 to 36	--	--
	36 to 48	--	--
Wooded area	0 to 6	--	--
	6 to 12	--	--
	12 to 24	--	--
	24 to 36	--	--
	36 to 48	--	--
Open area	0 to 6	--	--
	6 to 12	--	--
	12 to 24	--	--
	24 to 36	--	--
	36 to 48	--	--
Calibration lanes	0 to 6	13.6	--
	6 to 12	23.2	--
	12 to 24	26.3	--
	24 to 36	29.7	--
	36 to 48	38.9	--
Blind grid/moguls	0 to 6	--	10.6
	6 to 12	--	21.2
	12 to 24	--	24.1
	24 to 36	--	26.2
	36 to 48	--	32.7

Date: 23 Jun 09			
Probe Location	Layer, in.	AM Reading, %	PM Reading, %
Wet area	0 to 6	--	--
	6 to 12	--	--
	12 to 24	--	--
	24 to 36	--	--
	36 to 48	--	--
Wooded area	0 to 6	--	--
	6 to 12	--	--
	12 to 24	--	--
	24 to 36	--	--
	36 to 48	--	--
Open area	0 to 6	--	--
	6 to 12	--	--
	12 to 24	--	--
	24 to 36	--	--
	36 to 48	--	--
Calibration lanes	0 to 6	13.4	13.4
	6 to 12	23.6	23.6
	12 to 24	26.2	26.2
	24 to 36	30.7	30.7
	36 to 48	38.7	38.7
Blind grid/moguls	0 to 6	10.4	--
	6 to 12	21.1	--
	12 to 24	23.8	--
	24 to 36	26.0	--
	36 to 48	32.5	--

Date: 24 Jun 09			
Probe Location	Layer, in.	AM Reading, %	PM Reading, %
Wet area	0 to 6	--	--
	6 to 12	--	--
	12 to 24	--	--
	24 to 36	--	--
	36 to 48	--	--
Wooded area	0 to 6	--	--
	6 to 12	--	--
	12 to 24	--	--
	24 to 36	--	--
	36 to 48	--	--
Open area	0 to 6	--	--
	6 to 12	--	--
	12 to 24	--	--
	24 to 36	--	--
	36 to 48	--	--
Calibration lanes	0 to 6	--	--
	6 to 12	--	--
	12 to 24	--	--
	24 to 36	--	--
	36 to 48	--	--
Blind grid/moguls	0 to 6	10.2	10.1
	6 to 12	20.9	20.7
	12 to 24	23.6	23.5
	24 to 36	25.8	25.9
	36 to 48	32.7	32.8

Date: 25 Jun 09			
Probe Location	Layer, in.	AM Reading, %	PM Reading, %
Wet area	0 to 6	--	--
	6 to 12	--	--
	12 to 24	--	--
	24 to 36	--	--
	36 to 48	--	--
Wooded area	0 to 6	--	--
	6 to 12	--	--
	12 to 24	--	--
	24 to 36	--	--
	36 to 48	--	--
Open area	0 to 6	--	--
	6 to 12	--	--
	12 to 24	--	--
	24 to 36	--	--
	36 to 48	--	--
Calibration lanes	0 to 6	--	--
	6 to 12	--	--
	12 to 24	--	--
	24 to 36	--	--
	36 to 48	--	--
Blind grid/moguls	0 to 6	--	9.9
	6 to 12	--	20.6
	12 to 24	--	23.3
	24 to 36	--	25.8
	36 to 48	--	32.6

Date: 26 Jun 09			
Probe Location	Layer, in.	AM Reading, %	PM Reading, %
Wet area	0 to 6	--	--
	6 to 12	--	--
	12 to 24	--	--
	24 to 36	--	--
	36 to 48	--	--
Wooded area	0 to 6	--	--
	6 to 12	--	--
	12 to 24	--	--
	24 to 36	--	--
	36 to 48	--	--
Open area	0 to 6	--	--
	6 to 12	--	--
	12 to 24	--	--
	24 to 36	--	--
	36 to 48	--	--
Calibration lanes	0 to 6	--	--
	6 to 12	--	--
	12 to 24	--	--
	24 to 36	--	--
	36 to 48	--	--
Blind grid/moguls	0 to 6	9.6	9.6
	6 to 12	20.4	20.3
	12 to 24	23.1	23.0
	24 to 36	25.7	25.5
	36 to 48	32.4	32.4

Date: 29 Jun 09			
Probe Location	Layer, in.	AM Reading, %	PM Reading, %
Wet area	0 to 6	--	--
	6 to 12	--	--
	12 to 24	--	--
	24 to 36	--	--
	36 to 48	--	--
Wooded area	0 to 6	--	--
	6 to 12	--	--
	12 to 24	--	--
	24 to 36	--	--
	36 to 48	--	--
Open area	0 to 6	--	--
	6 to 12	--	--
	12 to 24	--	--
	24 to 36	--	--
	36 to 48	--	--
Calibration lanes	0 to 6	--	--
	6 to 12	--	--
	12 to 24	--	--
	24 to 36	--	--
	36 to 48	--	--
Blind grid/moguls	0 to 6	9.1	9.0
	6 to 12	19.8	19.8
	12 to 24	22.7	22.8
	24 to 36	25.3	25.1
	36 to 48	32.0	31.9

Date: 30 Jun 09			
Probe Location	Layer, in.	AM Reading, %	PM Reading, %
Wet area	0 to 6	--	--
	6 to 12	--	--
	12 to 24	--	--
	24 to 36	--	--
	36 to 48	--	--
Wooded area	0 to 6	--	--
	6 to 12	--	--
	12 to 24	--	--
	24 to 36	--	--
	36 to 48	--	--
Open area	0 to 6	--	--
	6 to 12	--	--
	12 to 24	--	--
	24 to 36	--	--
	36 to 48	--	--
Calibration lanes	0 to 6	12.5	15.7
	6 to 12	22.1	23.8
	12 to 24	25.7	27.9
	24 to 36	29.5	29.8
	36 to 48	37.9	38.6
Blind grid/moguls	0 to 6	--	--
	6 to 12	--	--
	12 to 24	--	--
	24 to 36	--	--
	36 to 48	--	--

Date: 01 Jul 09			
Probe Location	Layer, in.	AM Reading, %	PM Reading, %
Wet area	0 to 6	--	--
	6 to 12	--	--
	12 to 24	--	--
	24 to 36	--	--
	36 to 48	--	--
Wooded area	0 to 6	--	--
	6 to 12	--	--
	12 to 24	--	--
	24 to 36	--	--
	36 to 48	--	--
Open area	0 to 6	--	--
	6 to 12	--	--
	12 to 24	--	--
	24 to 36	--	--
	36 to 48	--	--
Calibration lanes	0 to 6	16.2	--
	6 to 12	24.8	--
	12 to 24	28.6	--
	24 to 36	31.5	--
	36 to 48	39.7	--
Blind grid/moguls	0 to 6	--	11.3
	6 to 12	--	22.5
	12 to 24	--	25.4
	24 to 36	--	27.8
	36 to 48	--	34.6

Date: 06 Jul 09			
Probe Location	Layer, in.	AM Reading, %	PM Reading, %
Wet area	0 to 6	--	--
	6 to 12	--	--
	12 to 24	--	--
	24 to 36	--	--
	36 to 48	--	--
Wooded area	0 to 6	--	--
	6 to 12	--	--
	12 to 24	--	--
	24 to 36	--	--
	36 to 48	--	--
Open area	0 to 6	--	--
	6 to 12	--	--
	12 to 24	--	--
	24 to 36	--	--
	36 to 48	--	--
Calibration lanes	0 to 6	--	--
	6 to 12	--	--
	12 to 24	--	--
	24 to 36	--	--
	36 to 48	--	--
Blind grid/moguls	0 to 6	10.8	10.8
	6 to 12	22.1	22.0
	12 to 24	24.7	24.5
	24 to 36	27.2	27.2
	36 to 48	34.1	34.0

Date: 07 Jul 09			
Probe Location	Layer, in.	AM Reading, %	PM Reading, %
Wet area	0 to 6	--	--
	6 to 12	--	--
	12 to 24	--	--
	24 to 36	--	--
	36 to 48	--	--
Wooded area	0 to 6	--	--
	6 to 12	--	--
	12 to 24	--	--
	24 to 36	--	--
	36 to 48	--	--
Open area	0 to 6	--	--
	6 to 12	--	--
	12 to 24	--	--
	24 to 36	--	--
	36 to 48	--	--
Calibration lanes	0 to 6	15.6	--
	6 to 12	24.2	--
	12 to 24	27.5	--
	24 to 36	30.2	--
	36 to 48	37.1	--
Blind grid/moguls	0 to 6	10.6	10.5
	6 to 12	21.8	21.7
	12 to 24	23.9	23.9
	24 to 36	26.9	26.6
	36 to 48	33.8	33.6

Date: 08 Jul 09			
Probe Location	Layer, in.	AM Reading, %	PM Reading, %
Wet area	0 to 6	--	--
	6 to 12	--	--
	12 to 24	--	--
	24 to 36	--	--
	36 to 48	--	--
Wooded area	0 to 6	--	--
	6 to 12	--	--
	12 to 24	--	--
	24 to 36	--	--
	36 to 48	--	--
Open area	0 to 6	--	--
	6 to 12	--	--
	12 to 24	--	--
	24 to 36	--	--
	36 to 48	--	--
Calibration lanes	0 to 6	--	15.3
	6 to 12	--	24.0
	12 to 24	--	27.1
	24 to 36	--	29.8
	36 to 48	--	36.8
Blind grid/moguls	0 to 6	10.3	10.2
	6 to 12	21.5	21.4
	12 to 24	23.8	23.6
	24 to 36	26.4	26.4
	36 to 48	33.3	33.3

Date, 2009	No. of People	Area-Tested	Status Start Time	Status Stop Time	Duration min.	Operational Status	Operational Status - Comments	Track Method	Pattern	Field Conditions	
										SUNNY	MUDDY
22 Jun	3	CALIBRATION LANES	0845	1030	105	INITIAL SET-UP	INITIAL MOBILIZATION, SAINT	GPS	LINEAR	SUNNY	MUDDY
	3	CALIBRATION LANES	1030	1140	70	COLLECTING DATA	COLLECTING DATA POINTS	GPS	LINEAR	SUNNY	MUDDY
	3	CALIBRATION LANES	1140	1230	50	BREAK/LUNCH	BREAK/LUNCH	GPS	LINEAR	SUNNY	MUDDY
	3	BLIND TEST GRID	1230	1615	225	COLLECTING DATA	COLLECTING DATA POINTS	GPS	LINEAR	SUNNY	MUDDY
	3	BLIND TEST GRID	1615	1640	25	DAILY START, STOP	EQUIPMENT BREAKDOWN	GPS	LINEAR	SUNNY	MUDDY
23 Jun	3	BLIND TEST GRID	0730	0750	20	DAILY START, STOP	SET UP EQUIPMENT	GPS	LINEAR	CLOUDY	MUDDY
	3	BLIND TEST GRID	0750	0845	55	COLLECTING DATA	COLLECTING DATA POINTS	GPS	LINEAR	CLOUDY	MUDDY
	3	CALIBRATION LANES	0845	0950	65	COLLECTING DATA	COLLECTING DATA POINTS, USING WOOD BOARD	POINTS	LINEAR	CLOUDY	MUDDY
	3	CALIBRATION LANES	0950	1020	30	DOWNTIME DUE TO EQUIP MAINT/CHECK	DOWNLOAD DATA	POINTS	LINEAR	CLOUDY	MUDDY
	3	CALIBRATION LANES	1020	1155	95	COLLECTING DATA	COLLECTING DATA POINTS, USING WOOD BOARD	POINTS	LINEAR	CLOUDY	MUDDY
	3	CALIBRATION LANES	1155	1210	15	DOWNTIME DUE TO EQUIP MAINT/CHECK	DOWNLOAD DATA	POINTS	LINEAR	CLOUDY	MUDDY
	3	CALIBRATION LANES	1210	1240	30	BREAK/LUNCH	BREAK/LUNCH	POINTS	LINEAR	CLOUDY	MUDDY
	3	CALIBRATION LANES	1240	1325	45	COLLECTING DATA	COLLECTING DATA POINTS, USING WOOD BOARD	POINTS	LINEAR	CLOUDY	MUDDY
	3	CALIBRATION LANES	1325	1340	15	DOWNTIME DUE TO EQUIP MAINT/CHECK	DOWNLOAD DATA	POINTS	LINEAR	CLOUDY	MUDDY
	3	CALIBRATION LANES	1340	1420	40	COLLECTING DATA	COLLECTING DATA POINTS, USING WOOD BOARD	POINTS	LINEAR	CLOUDY	MUDDY
	3	CALIBRATION LANES	1420	1435	15	DOWNTIME DUE TO EQUIP MAINT/CHECK	DOWNLOAD DATA	POINTS	LINEAR	CLOUDY	MUDDY
	3	CALIBRATION LANES	1435	1510	35	COLLECTING DATA	COLLECTING DATA POINTS, USING WOOD BOARD	POINTS	LINEAR	CLOUDY	MUDDY
	3	CALIBRATION LANES	1510	1520	10	DOWNTIME DUE TO EQUIP MAINT/CHECK	DOWNLOAD DATA	POINTS	LINEAR	CLOUDY	MUDDY
	3	CALIBRATION LANES	1520	1600	40	COLLECTING DATA	COLLECTING DATA POINTS, USING WOOD BOARD	POINTS	LINEAR	CLOUDY	MUDDY
	3	CALIBRATION LANES	1600	1610	10	DOWNTIME DUE TO EQUIP MAINT/CHECK	DOWNLOAD DATA	POINTS	LINEAR	CLOUDY	MUDDY
	3	CALIBRATION LANES	1610	1640	30	DAILY START, STOP	EQUIPMENT BREAKDOWN	POINTS	LINEAR	CLOUDY	MUDDY

Date, 2009	No. of People	Area-Tested	Status Start Time	Status Stop Time	Duration min.	Operational Status	Operational Status - Comments	Track Method	Pattern	Field Conditions	
24 Jun	3	BLIND TEST GRID	0745	0805	20	DAILY START, STOP	SET UP EQUIPMENT	POINTS	LINEAR	SUNNY	MUDDY
	3	BLIND TEST GRID	0805	0930	85	COLLECTING DATA	COLLECTING DATA POINTS, USING WOOD BOARD	POINTS	LINEAR	SUNNY	MUDDY
	3	BLIND TEST GRID	0930	0945	15	DOWNTIME DUE TO EQUIP MAINT/CHECK	DOWNLOAD DATA	POINTS	LINEAR	SUNNY	MUDDY
	3	BLIND TEST GRID	0945	1050	65	COLLECTING DATA	COLLECTING DATA POINTS, USING WOOD BOARD	POINTS	LINEAR	SUNNY	MUDDY
	3	BLIND TEST GRID	1050	1105	15	DOWNTIME DUE TO EQUIP MAINT/CHECK	DOWNLOAD DATA	POINTS	LINEAR	SUNNY	MUDDY
	3	BLIND TEST GRID	1105	1215	70	COLLECTING DATA	COLLECTING DATA POINTS, USING WOOD BOARD	POINTS	LINEAR	SUNNY	MUDDY
	3	BLIND TEST GRID	1215	1225	10	DOWNTIME DUE TO EQUIP MAINT/CHECK	DOWNLOAD DATA	POINTS	LINEAR	SUNNY	MUDDY
	3	BLIND TEST GRID	1225	1305	40	BREAK/LUNCH	BREAK/LUNCH	POINTS	LINEAR	SUNNY	MUDDY
	3	BLIND TEST GRID	1305	1425	80	COLLECTING DATA	COLLECTING DATA POINTS, USING WOOD BOARD	POINTS	LINEAR	SUNNY	MUDDY
	3	BLIND TEST GRID	1425	1440	15	DOWNTIME DUE TO EQUIPMENT FAILURE	LOOSE CABLE TO BE REPAIRED	POINTS	LINEAR	SUNNY	MUDDY
	3	BLIND TEST GRID	1440	1515	35	DAILY START, STOP	EQUIPMENT BREAKDOWN	POINTS	LINEAR	SUNNY	MUDDY
25 Jun	3	BLIND TEST GRID	1115	1140	25	DAILY START, STOP	SET UP EQUIPMENT	POINTS	LINEAR	SUNNY	MUDDY
	3	BLIND TEST GRID	1140	1245	65	COLLECTING DATA	COLLECTING DATA POINTS, USING WOOD BOARD	POINTS	LINEAR	SUNNY	MUDDY
	3	BLIND TEST GRID	1245	1300	15	DOWNTIME DUE TO EQUIP MAINT/CHECK	DOWNLOAD DATA	POINTS	LINEAR	SUNNY	MUDDY
	3	BLIND TEST GRID	1300	1400	60	COLLECTING DATA	COLLECTING DATA POINTS, USING WOOD BOARD	POINTS	LINEAR	SUNNY	MUDDY
	3	BLIND TEST GRID	1400	1420	20	DOWNTIME DUE TO EQUIP MAINT/CHECK	DOWNLOAD DATA	POINTS	LINEAR	SUNNY	MUDDY
	3	BLIND TEST GRID	1420	1620	120	COLLECTING DATA	COLLECTING DATA POINTS, USING WOOD BOARD	POINTS	LINEAR	SUNNY	MUDDY
	3	BLIND TEST GRID	1620	1635	15	DOWNTIME DUE TO EQUIP MAINT/CHECK	DOWNLOAD DATA	POINTS	LINEAR	SUNNY	MUDDY
	3	BLIND TEST GRID	1635	1655	20	DAILY START, STOP	EQUIPMENT BREAKDOWN	POINTS	LINEAR	SUNNY	MUDDY

Date, 2009	No. of People	Area-Tested	Status Start Time	Status Stop Time	Duration min.	Operational Status	Operational Status - Comments	Track Method	Pattern	Field Conditions	
26 Jun	3	BLIND TEST GRID	0745	0805	20	DAILY START, STOP	SET UP EQUIPMENT	POINTS	LINEAR	CLOUDY	MUDDY
	3	BLIND TEST GRID	0805	0915	70	COLLECTING DATA	COLLECTING DATA POINTS, USING WOOD BOARD	POINTS	LINEAR	CLOUDY	MUDDY
	3	BLIND TEST GRID	0915	0925	10	DOWNTIME DUE TO EQUIP MAINT/CHECK	DATA CHECK	POINTS	LINEAR	CLOUDY	MUDDY
	3	BLIND TEST GRID	0925	1200	155	COLLECTING DATA	COLLECTING DATA POINTS, USING WOOD BOARD	POINTS	LINEAR	CLOUDY	MUDDY
	3	BLIND TEST GRID	1200	1210	10	DOWNTIME DUE TO EQUIP MAINT/CHECK	DOWNLOAD DATA	POINTS	LINEAR	CLOUDY	MUDDY
	3	BLIND TEST GRID	1210	1235	25	BREAK/LUNCH	BREAK/LUNCH	POINTS	LINEAR	CLOUDY	MUDDY
	3	BLIND TEST GRID	1235	1545	190	COLLECTING DATA	COLLECTING DATA POINTS, USING WOOD BOARD	POINTS	LINEAR	CLOUDY	MUDDY
	3	BLIND TEST GRID	1545	1600	15	DAILY START, STOP	EQUIPMENT BREAKDOWN	POINTS	LINEAR	CLOUDY	MUDDY
29 Jun	3	BLIND TEST GRID	0745	0800	15	DAILY START, STOP	SET UP EQUIPMENT	POINTS	LINEAR	SUNNY	MUDDY
	3	BLIND TEST GRID	0800	1145	225	COLLECTING DATA	COLLECTING DATA POINTS, USING WOOD BOARD	POINTS	LINEAR	SUNNY	MUDDY
	3	BLIND TEST GRID	1145	1200	15	DOWNTIME DUE TO EQUIP MAINT/CHECK	DOWNLOAD DATA	POINTS	LINEAR	SUNNY	MUDDY
	3	BLIND TEST GRID	1200	1240	40	BREAK/LUNCH	BREAK/LUNCH	POINTS	LINEAR	SUNNY	MUDDY
	3	BLIND TEST GRID	1240	1635	235	COLLECTING DATA	COLLECTING DATA POINTS, USING WOOD BOARD	POINTS	LINEAR	SUNNY	MUDDY
	3	BLIND TEST GRID	1635	1645	10	DOWNTIME DUE TO EQUIP MAINT/CHECK	DOWNLOAD DATA	POINTS	LINEAR	SUNNY	MUDDY
	3	BLIND TEST GRID	1645	1700	15	DAILY START, STOP	EQUIPMENT BREAKDOWN	POINTS	LINEAR	SUNNY	MUDDY
8 Jul	3	CALIBRATION LANES	1405	1420	15	DAILY START, STOP	SET UP EQUIPMENT	POINTS	LINEAR	SUNNY	MUDDY
	3	CALIBRATION LANES	1420	1450	30	COLLECTING DATA	COLLECTING DATA POINTS, USING WOOD BOARD	POINTS	LINEAR	SUNNY	MUDDY
	3	CALIBRATION LANES	1450	1505	15	DAILY START, STOP	EQUIPMENT BREAKDOWN	POINTS	LINEAR	SUNNY	MUDDY
	3	CALIBRATION LANES	0840	0945	65	DEMOBILIZATION	DEMOBILIZATION	POINTS	LINEAR	SUNNY	MUDDY

Date, 2009	No. of People	Area-Tested	Status Start Time	Status Stop Time	Duration min.	Operational Status	Operational Status - Comments	Track Method	Pattern	Field Conditions	
NEW DATA COLLECTION METHOD, WOODEN PLATFORM											
22 Jun	3	CALIBRATION LANES	0845	1030	105	INITIAL SET-UP	INITIAL MOBILIZATION	GPS	LINEAR	SUNNY	MUDDY
	3	CALIBRATION LANES	1030	1140	70	COLLECTING DATA	COLLECTING DATA POINTS	GPS	LINEAR	SUNNY	MUDDY
	3	CALIBRATION LANES	1140	1230	50	BREAK/LUNCH	BREAK/LUNCH	GPS	LINEAR	SUNNY	MUDDY
	3	BLIND TEST GRID	1230	1615	225	COLLECTING DATA	COLLECTING DATA POINTS	GPS	LINEAR	SUNNY	MUDDY
	3	BLIND TEST GRID	1615	1640	25	DAILY START, STOP	EQUIPMENT BREAKDOWN	GPS	LINEAR	SUNNY	MUDDY
23 Jun	3	BLIND TEST GRID	0730	0750	20	DAILY START, STOP	SET UP EQUIPMENT	GPS	LINEAR	CLOUDY	MUDDY
	3	BLIND TEST GRID	0750	0845	55	COLLECTING DATA	COLLECTING DATA POINTS	GPS	LINEAR	CLOUDY	MUDDY
30 Jun	3	CALIBRATION LANES	0745	0810	5	DAILY START, STOP	SET UP EQUIPMENT	POINTS	LINEAR	SUNNY	MUDDY
	3	CALIBRATION LANES	0810	1025	135	COLLECTING DATA	COLLECTING DATA POINTS, USING WOOD PLATFORM	POINTS	LINEAR	SUNNY	MUDDY
	3	CALIBRATION LANES	1025	1030	5	DOWNTIME DUE TO EQUIP MAINT/CHECK	DATA CHECK	POINTS	LINEAR	SUNNY	MUDDY
	3	CALIBRATION LANES	1030	1205	95	COLLECTING DATA	COLLECTING DATA POINTS, USING WOOD PLATFORM	POINTS	LINEAR	SUNNY	MUDDY
	3	CALIBRATION LANES	1205	1215	10	DOWNTIME DUE TO EQUIP MAINT/CHECK	DOWNLOAD DATA	POINTS	LINEAR	SUNNY	MUDDY
	3	CALIBRATION LANES	1215	1255	40	BREAK/LUNCH	BREAK/LUNCH	POINTS	LINEAR	SUNNY	MUDDY
	3	CALIBRATION LANES	1255	1340	45	COLLECTING DATA	COLLECTING DATA POINTS, USING WOOD PLATFORM	POINTS	LINEAR	SUNNY	MUDDY
	3	CALIBRATION LANES	1340	1530	110	WEATHER ISSUE	LIGHTNING ADVISORY	POINTS	LINEAR	SUNNY	MUDDY
	3	CALIBRATION LANES	1530	1630	60	COLLECTING DATA	COLLECTING DATA POINTS, USING WOOD PLATFORM	POINTS	LINEAR	SUNNY	MUDDY
	3	CALIBRATION LANES	1630	1640	10	DOWNTIME DUE TO EQUIP MAINT/CHECK	DOWNLOAD DATA	POINTS	LINEAR	SUNNY	MUDDY
3	CALIBRATION LANES	1640	1650	10	DAILY START, STOP	EQUIPMENT BREAKDOWN	POINTS	LINEAR	SUNNY	MUDDY	

Date, 2009	No. of People	Area-Tested	Status Start Time	Status Stop Time	Duration min.	Operational Status	Operational Status - Comments	Track Method	Pattern	Field Conditions	
1 Jul	3	CALIBRATION LANES	0740	0755	15	DAILY START, STOP	SET UP EQUIPMENT	GPS	LINEAR	CLOUDY	MUDDY
	3	CALIBRATION LANES	0755	1130	215	COLLECTING DATA	COLLECTING DATA POINTS, USING WOOD PLATFORM	GPS	LINEAR	CLOUDY	MUDDY
	3	CALIBRATION LANES	1130	1230	60	BREAK/LUNCH	BREAK/LUNCH	GPS	LINEAR	CLOUDY	MUDDY
	3	BLIND TEST GRID	1230	1620	230	COLLECTING DATA	COLLECTING DATA POINTS, USING WOOD PLATFORM	GPS	LINEAR	CLOUDY	MUDDY
	3	BLIND TEST GRID	1620	1630	10	DAILY START, STOP	EQUIPMENT BREAKDOWN	GPS	LINEAR	CLOUDY	MUDDY
6 Jul	3	BLIND TEST GRID	0755	0815	20	DAILY START, STOP	SET UP EQUIPMENT	POINTS	LINEAR	SUNNY	MUDDY
	3	BLIND TEST GRID	0815	1205	230	COLLECTING DATA	COLLECTING DATA POINTS, USING WOOD PLATFORM	POINTS	LINEAR	SUNNY	MUDDY
	3	BLIND TEST GRID	1205	1250	45	BREAK/LUNCH	BREAK/LUNCH	POINTS	LINEAR	SUNNY	MUDDY
	3	BLIND TEST GRID	1250	1545	175	COLLECTING DATA	COLLECTING DATA POINTS, USING WOOD PLATFORM	POINTS	LINEAR	SUNNY	MUDDY
	3	BLIND TEST GRID	1545	1600	15	DAILY START, STOP	EQUIPMENT BREAKDOWN	POINTS	LINEAR	SUNNY	MUDDY
7 Jul	3	CALIBRATION LANES	0835	0855	20	DAILY START, STOP	SET UP EQUIPMENT	POINTS	LINEAR	SUNNY	MUDDY
	3	CALIBRATION LANES	0855	0930	35	COLLECTING DATA	COLLECTING DATA POINTS, USING WOOD PLATFORM	POINTS	LINEAR	SUNNY	MUDDY
	3	BLIND TEST GRID	0930	1115	105	COLLECTING DATA	COLLECTING DATA POINTS, USING WOOD PLATFORM	POINTS	LINEAR	SUNNY	MUDDY
	3	BLIND TEST GRID	1115	1305	110	DEMONSTRATION SITE ISSUE	DEMONSTRATOR OFF RANGE	POINTS	LINEAR	SUNNY	MUDDY
	3	BLIND TEST GRID	1305	1625	200	COLLECTING DATA	COLLECTING DATA POINTS, USING WOOD PLATFORM	POINTS	LINEAR	SUNNY	MUDDY
	3	BLIND TEST GRID	1625	1640	15	DAILY START, STOP	EQUIPMENT BREAKDOWN	POINTS	LINEAR	SUNNY	MUDDY
8 Jul	3	BLIND TEST GRID	0740	0800	20	DAILY START, STOP	SET UP EQUIPMENT	POINTS	LINEAR	SUNNY	MUDDY
	3	BLIND TEST GRID	0800	1205	245	COLLECTING DATA	COLLECTING DATA POINTS, USING WOOD PLATFORM	POINTS	LINEAR	SUNNY	MUDDY
	3	BLIND TEST GRID	1205	1255	50	BREAK/LUNCH	BREAK/LUNCH	POINTS	LINEAR	SUNNY	MUDDY
	3	BLIND TEST GRID	1255	1405	70	COLLECTING DATA	COLLECTING DATA POINTS, USING WOOD PLATFORM	POINTS	LINEAR	SUNNY	MUDDY
9 Jul	3	BLIND TEST GRID	0840	0945	65	DEMOBILIZATION	DEMOBILIZATION	POINTS	LINEAR	SUNNY	MUDDY

APPENDIX E. REFERENCES

1. Standardized UXO Technology Demonstration Site Handbook, DTC Project No. 8-CO-160-000-473, Report No. ATC-8349, March 2002.
2. Aberdeen Proving Ground Soil Survey Report, October 1998.
3. Data Summary, UXO Standardized Test Site: APG Soils Description, May 2002.

APPENDIX F. ABBREVIATIONS

ADST	=	Aberdeen Data Services Team
APG	=	Aberdeen Proving Ground
ATC	=	U.S. Army Aberdeen Test Center
ATSS	=	Aberdeen Test Support Services
BAR	=	background alarm rate
DMC	=	digital magnetic compass
DMM	=	discarded military munitions
EMI	=	electromagnetic interference
EQT	=	Environmental Quality Technology
ERDC	=	U.S. Army Corps of Engineers Engineering Research and Development Center
EST	=	Eastern Standard Time
ESTCP	=	Environmental Security Technology Certification Program
GPS	=	Global Positioning System
GT	=	ground truth
GUI	=	graphical user interface
HDSD	=	Homeland Defense and Sustainment Division
HEAT	=	high-explosive antitank
IMU	=	inertial measurement unit
JPG	=	Jefferson Proving Ground
MEMS	=	micro electro-mechanical systems
MM	=	military munitions
NA	=	not available
NS	=	nonstandard munition
PC	=	personal computer
POC	=	point of contact
QA	=	quality assurance
QC	=	quality control
ROC	=	receiver-operating characteristic
S	=	standard munition
SAIC	=	Science Applications International Corporation
SAINT	=	small area inertial navigation system
SCEMP	=	Simplified Combined EMI Magnetometer Prototype
SERDP	=	Strategic Environmental Research and Development Program
USAEC	=	U.S. Army Environmental Command
UXO	=	unexploded ordnance
YPG	=	U.S. Army Yuma Proving Ground
ZUPT	=	zero velocity update

Secondary distribution is controlled by Program Manager, SERDP/ESTCP, Munitions Management, ATTN: Mr. Herb Nelson.